



Kompozit Malzemeler

**Metal Matrisli
Kompozitler**

Metal Matrisli Kompozitler

Table 6.1 Typical reinforcements used in metal matrix composites

Type	Aspect ratio	Diameter (μm)	Examples
Particle	$\sim 1-4$	1–25	SiC, Al_2O_3 , WC, TiC, BN, B_4C
Short fiber or whisker	$\sim 10-1,000$	0.1–25	SiC, Al_2O_3 , $\text{Al}_2\text{O}_3 + \text{SiO}_2$, C
Continuous fiber	$> 1,000$	3–150	SiC, Al_2O_3 , $\text{Al}_2\text{O}_3 + \text{SiO}_2$, C, B, W, NbTi, Nb_3Sn

Ticari olarak kullanılan önemli metal matris malzemeleri:

Alüminyum alaşımları

Magnezyum alaşımları

Titanyum alaşımları

Nikel esaslı alaşımlar

Bakır alaşımları

Tungsten / Molibden gibi refrakter metaller

İntermetalikler

Metal Matrisli Kompozitler

TABLE 3.9

Typical Properties of Some Common Metallic Matrix Materials

Matrix	Density (g cm ⁻³)	Tensile Modulus (GPa)	Tensile Strength (MPa)	Strain to Failure (%)	CTE (10 ⁻⁶ °C ⁻¹)	Melting Point (°C)
<i>Al alloys</i>						
2024-T6	2.78	70	580	11	23.2	
6061-T6	2.70	70	310	17	23.6	
7075-T6	2.80	70	572	11	23.6	
8009	2.92	88	448	17	23.5	
380 (as cast)	2.71	70	330	4	—	540
<i>Ti alloy</i>						
Ti-6Al-4V	4.43	110	1170	8	9.5	1650
<i>Mg alloy</i>						
AZ91A	1.81	45	235	3	26	650
<i>Zinc–aluminum alloy</i>						
ZA-27	5	78	425	3	26	375
<i>Ni alloys</i>	8.8	200	460	47	13.3	1450
<i>Cu alloys</i>	8.9	100	200–500	5–60	18	1080
<i>Steel</i>	7.85	207	400–500	15–30	11.7	1500
<i>Intermetallics</i>						
FeAl	5.6	263	550 ^a	0.7 ^a	17	1400
NiAl	5.9	190	250	0.3	13.2	1680
TiAl	3.9	94	538	0.3	—	1460
MoSi ₂	6.3	430	325 ^b	—	8.5	2030

Source: Data from Mallick, P.K., *Fiber-Reinforced Composites*, 3rd edn., CRC Press, Boca Raton, FL, 2008, p. 525.

^a Furnace cool.

^b Bend strength of HIPed sample.

2000 serisi – Al-Cu-Mg

6000 serisi – Al-Mg-Si

7000 serisi – Al-Zn-Mg

Metal Matrisli Kompozitlerin Üretimi

Takviye elemanları matris malzemesine çeşitli şekillerde karıştırılır:

- 1- Enjeksiyon tabancası kullanarak inert gazların taşıyıcı olarak kullanılması
- 2- Kalıbın doldurulması sırasında partiküllerin ergiye karıştırılması ile
- 3- Mekanik karıştırma yardımıyla oluşturulan vortekse eklenerek
- 4- Önceden hazırlanmış yüksek oranda partikül içeren kompozitlerin eklenmesi sonrası karıştırma ile
- 5- Santrifüj dökümü ile
- 6- Ultrasonik titreşim ile

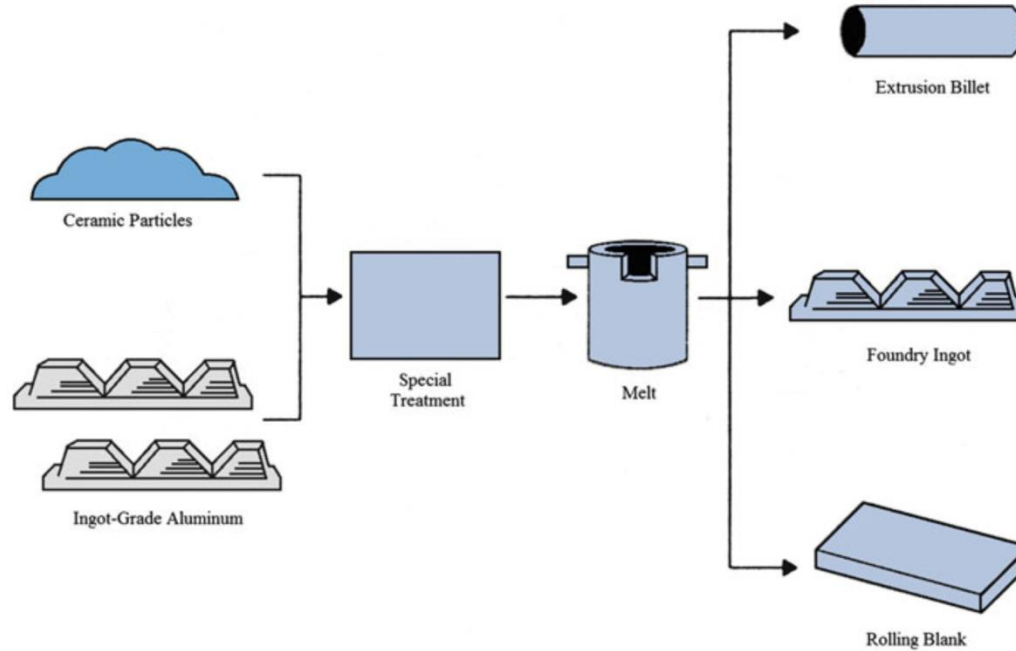


Fig. 6.2 Schematic of the Duralcan process

Metal Matrisli Kompozitlerin Üretimi

Karıştırırmalı Döküm

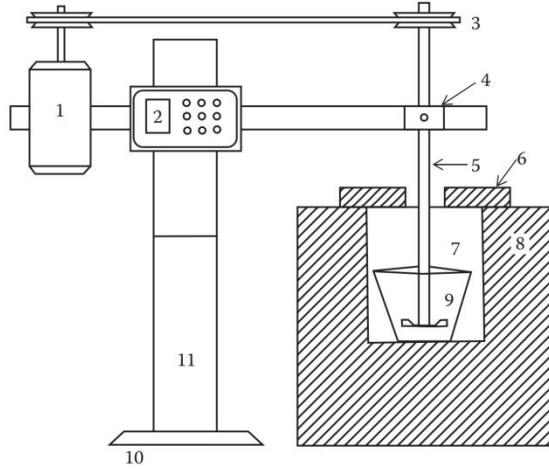


FIGURE 5.1
Schematic of stir casting process. 1. Variable speed motor, 2. speed controller, 3. pulley drive, 4. bearing assembly, 5. stirrer shaft, 6. insulating cover, 7. melting crucible, 8. furnace, 9. impeller, 10. base, 11. pedestal.

Santrifüjlü Döküm

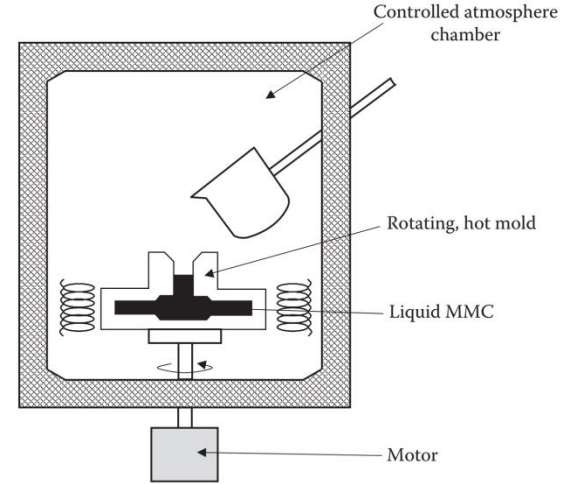


FIGURE 5.2
Schematic of centrifugal casting process. (Reprinted from Chawla, N. and Chawla, K.K., *Metal Matrix Composites*, Springer-Verlag, Inc., New York, 2006, p. 68. With permission.)

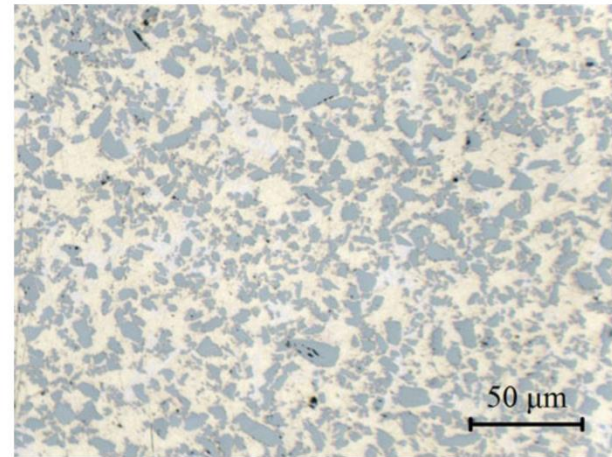


Fig. 6.6 Microstructure of a centrifugally cast WC/bronze composite

Metal Matrisli Kompozitlerin Üretimi

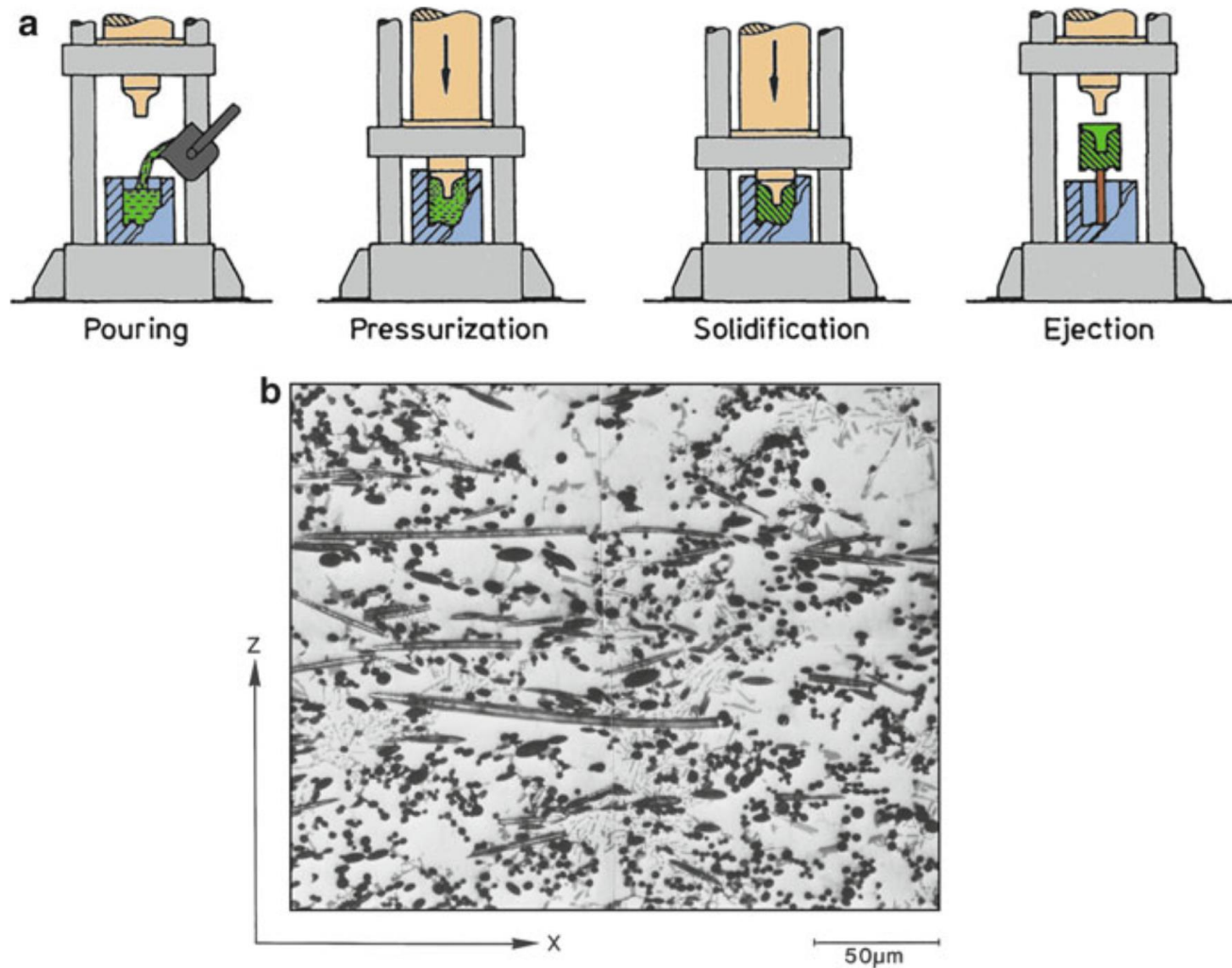


Fig. 6.5 (a) Squeeze casting technique of making a metal matrix composite. (b) The microstructure of Saffil alumina fiber/aluminum matrix composite made by squeeze casting. [Courtesy of G. Eggeler]

Metal Matrisli Kompozitlerin Üretimi

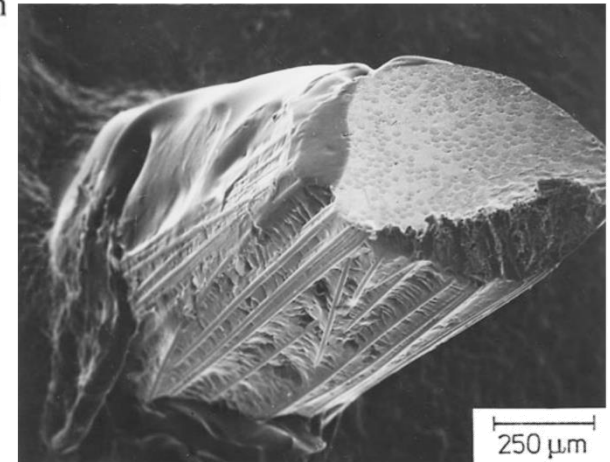
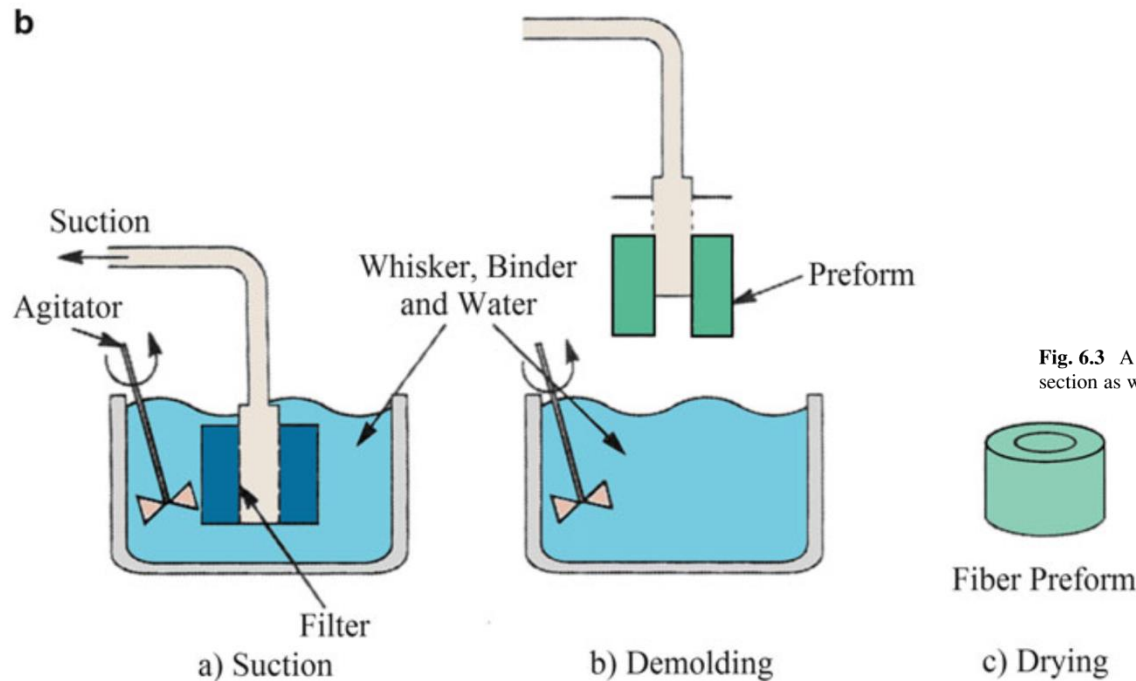
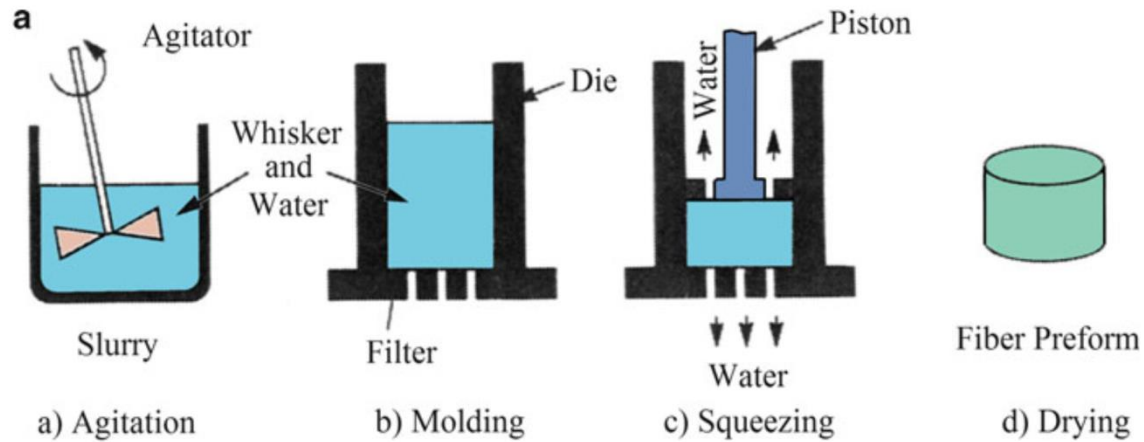


Fig. 6.3 A silicon carbide fiber/aluminum wire preform. SiC fibers can be seen in the transverse section as well as along the length the wire preform

Fig. 6.4 (a) Press forming of a preform. (b) Suction forming of a preform

Metal Matrisli Kompozitlerin Üretimi

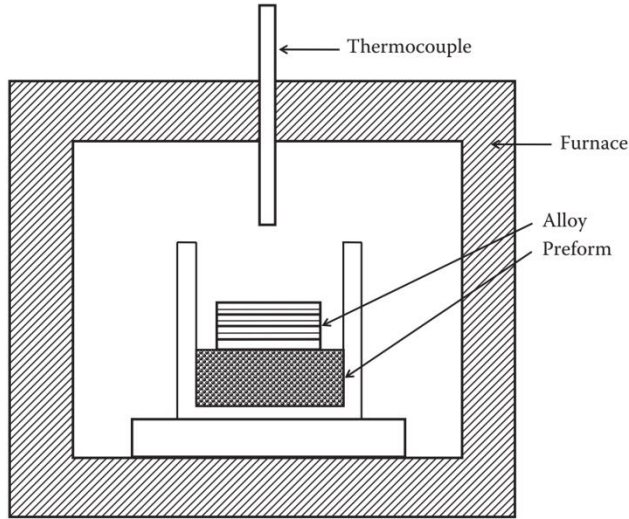


FIGURE 5.5
Schematic of spontaneous melt infiltration process. (Adapted from Agarwal, A. et al., *Carbon Nanotubes: Reinforced Metal Matrix Composites*, CRC Press, Boca Raton, FL, 2010, p. 33. With permission.)

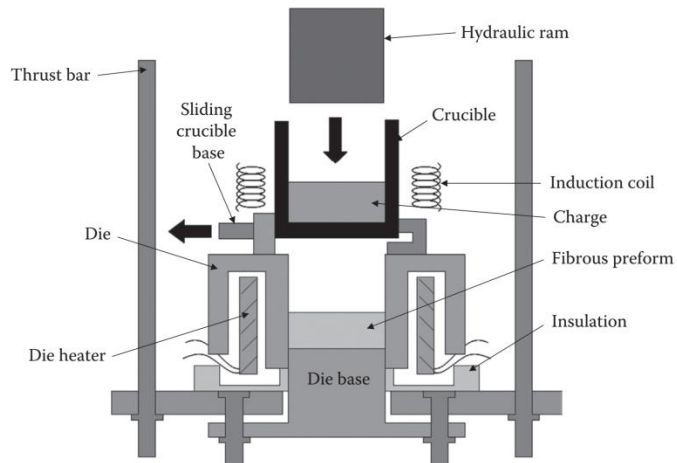


FIGURE 5.6
Schematic of squeeze infiltration process. (Reprinted from Clyne, T.W. and Withers, P.J., *An Introduction to Metal Matrix Composites*, Cambridge University Press, Cambridge, U.K., 1993, p. 325. With permission.)

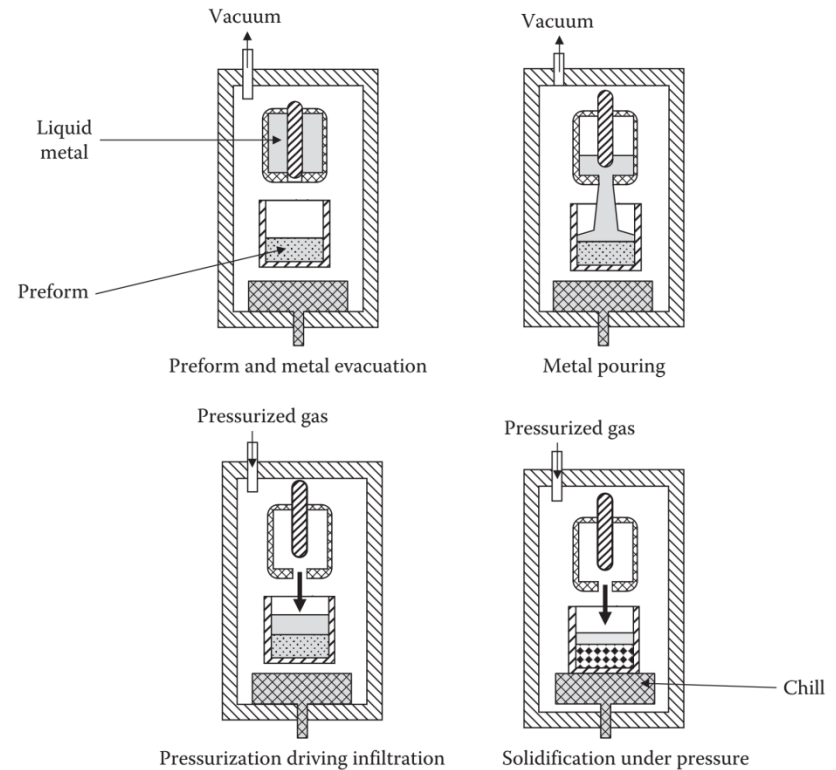


FIGURE 5.7
Schematic of a gas-driven pressure infiltration process. (Reprinted from Clyne, T.W., in *Comprehensive Composite Materials*, Vol. 3, eds. A. Kelly and C. Zweben, Elsevier Science Ltd., Oxford, U.K., 2000, p. 545. With permission.)

Metal Matrisli Kompozitlerin Üretimi

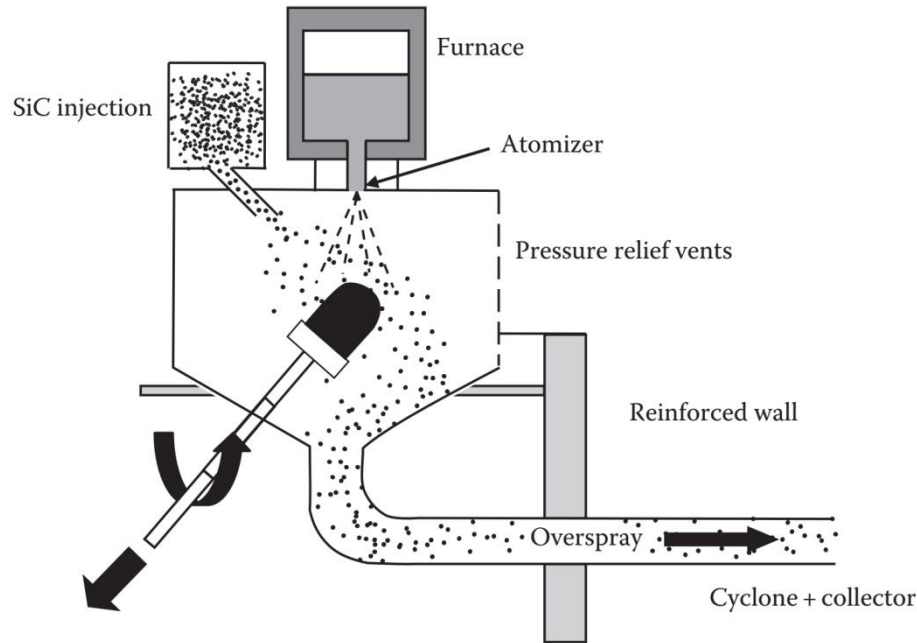
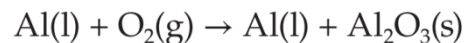
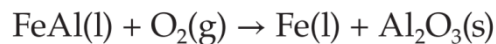
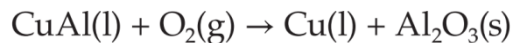
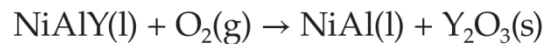
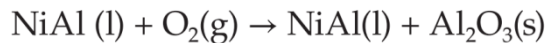


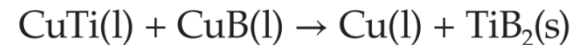
FIGURE 5.8

Schematic of a spray deposition arrangement for MMC manufacture. (Reprinted from Willis, T.C., *Metals Mater.*, 1988, 4, 485. With permission.)

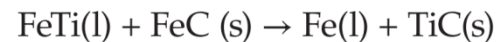
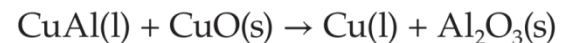
Sıvı-Gaz reaksiyonu



Sıvı-Sıvı reaksiyonu



Sıvı-Katı reaksiyonu



Metal Matrisli Kompozitlerin Üretimi

Arayüzey reaksiyonları ile bağlanma

Table 6.3 Interfacial reaction products in some important MMCs

Reinforcement	Matrix	Reaction product(s)
SiC	Ti alloy	TiC, Ti_5Si_3
	Al alloy	Al_4C_3
Al_2O_3	Mg alloy	MgO, $MgAl_2O_4$ (spinel)
C	Al alloy	Al_4C_3
B	Al alloy	AlB_2
$Al_2O_3 + ZrO_2$	Al alloy	$ZrAl_3$
W	Cu	None
C	Cu	None
Al_2O_3	Al	None

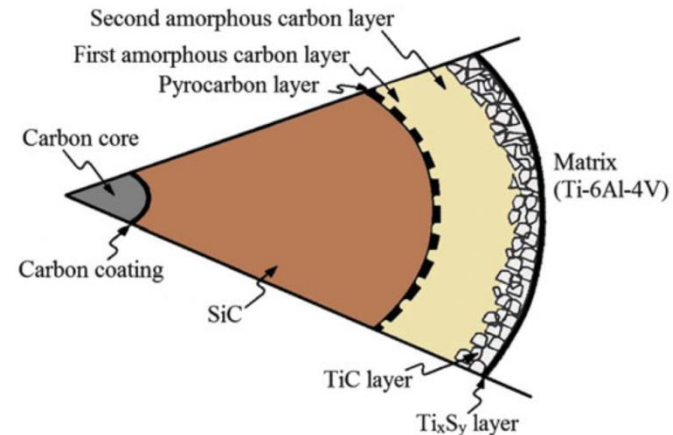
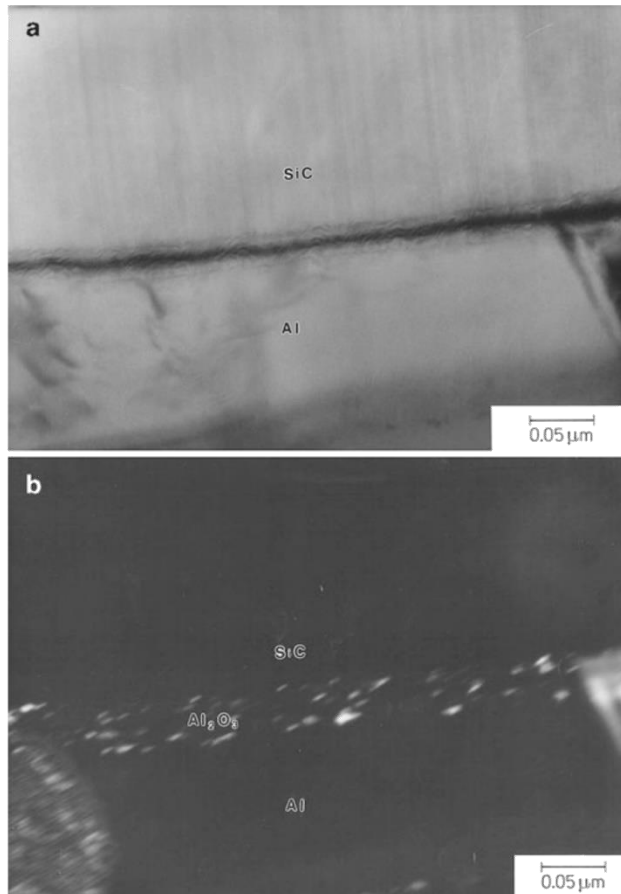


Fig. 6.13 Schematic of the interface region in silicon carbide fiber reinforced titanium matrix composites. [Adapted from Gabryel and McLeod (1991)]

Fig. 6.18 Interface in SiC_w/Al composite: (a) bright field TEM, (b) dark field TEM showing the presence of Al_2O_3 at the interface. [From Fu et al. (1986), ©ASTM, reprinted with permission]

Metal Matrisli Kompozitlerin Üretimi

**Katı hal prosesleri:
Difüzyonla bağlanma**

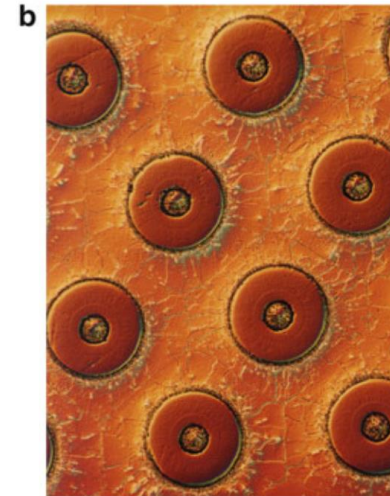
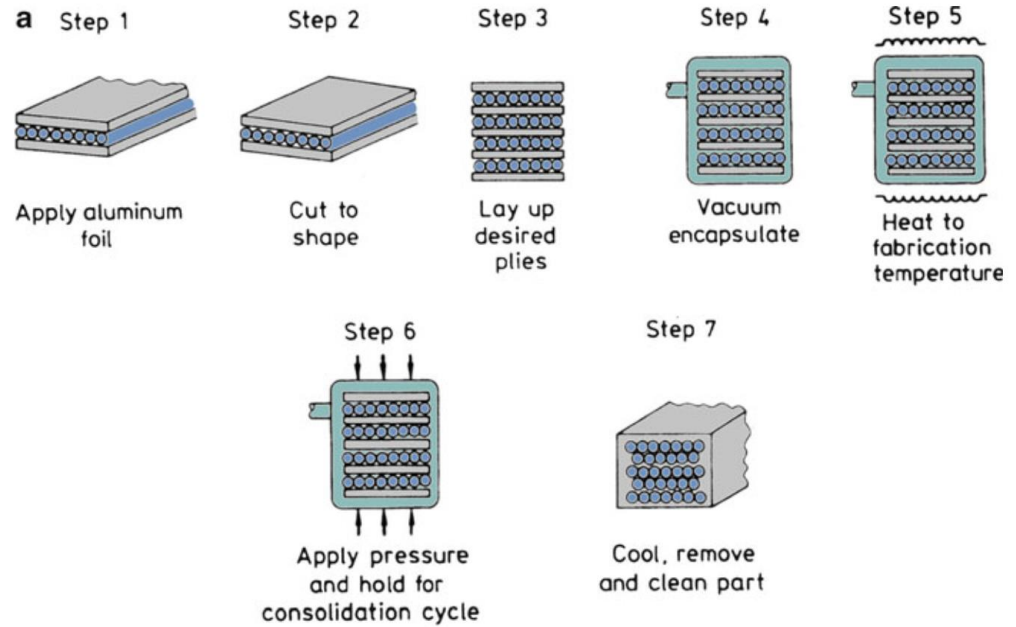


Fig. 6.8 (a) Schematic of diffusion bonding process. (b) The microstructure of SiC fiber/titanium matrix composite made by diffusion. Each fiber is 142 μm in diameter. [Courtesy of J. Baughman]

MMK Üretimi: Toz Metalurjisi

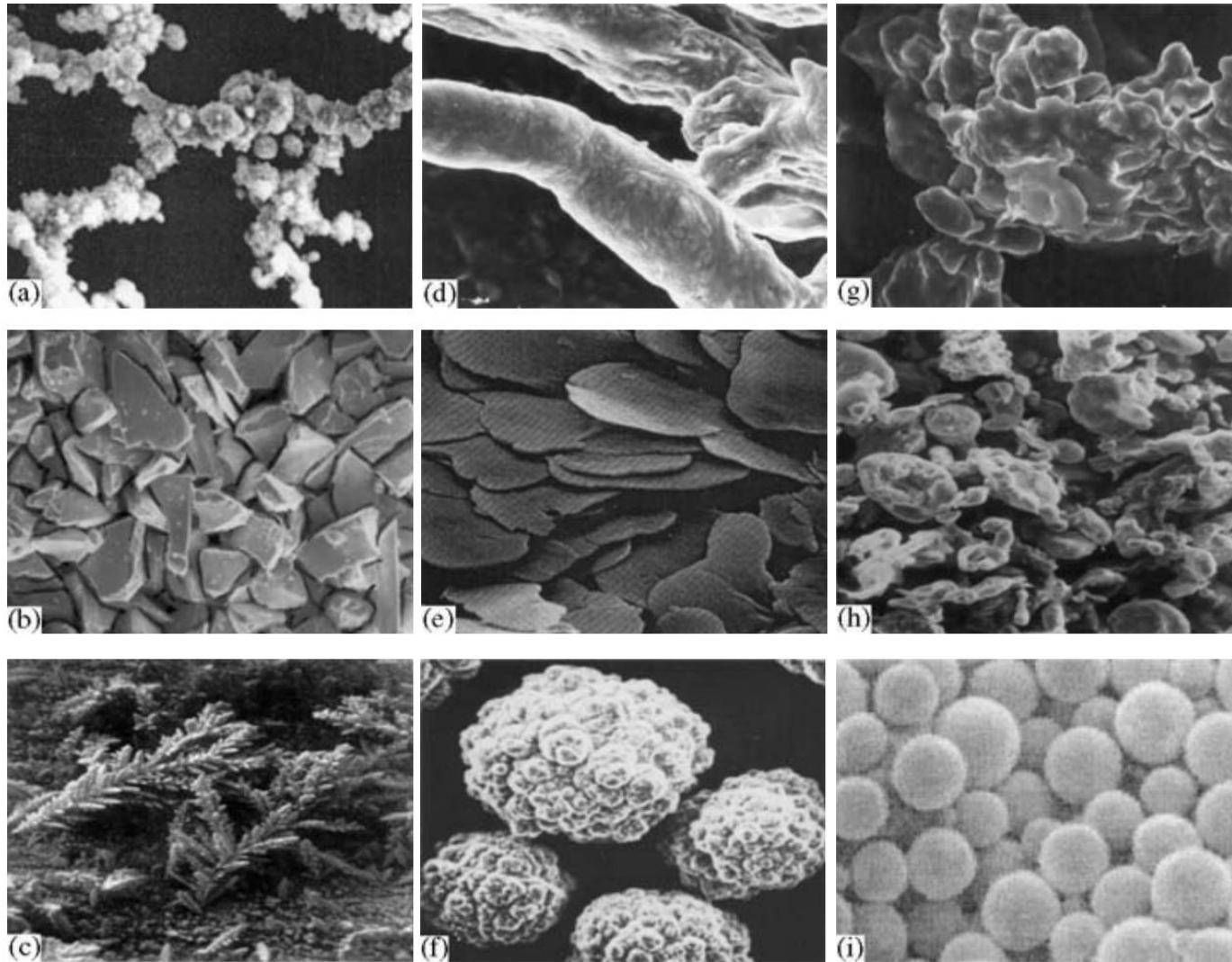


Figure 1.2 Characteristic particle shapes: (a) acicular powder particles; (b) angular powder particles; (c) dendritic powder particles; (d) fibrous powder particles; (e) flake powder particles; (f) granular powder particles; (g) Irregular powder particles; (h) nodular powder particles; (i) spheroidal powder particles.

MMK Üretimi: Toz Metalurjisi

Toz üretimi



Toz karakterizasyonu

Karıştırma/Harmanlama

İşleme / Presleme



Sinterleme

Yüzey İşlemleri



Son ürün P/M parçalar

MMK Üretimi: Toz Metalurjisi

Maliyet Avantajları:

- Sıfıra yakın atık ve hurda
- Karmaşık şekilli ürünlerin tek seferde üretilebilmesi sayesinde yüksek maliyetli son işlemlerden tasarruf
- Çok düşük maliyetlerle pürüzsüz yüzeyler elde edilebilmesi
- Herhangi bir talaşlı işleme gerek kalmadan istenilen boyutlarda (tolerans değerleri içerisinde) malzeme üretimi
- Geleneksel yöntemlerle iki veya daha fazla bileşen içeren parçaların tek seferde üretilebilmesi
- Aynı bileşenin farklı parçalarının sinterleme işleminden önce birleştirilebilme imkanı
- Yüksek üretim hızları

MMK Üretimi: Toz Metalurjisi

Ürün Özellikleri Avantajları:

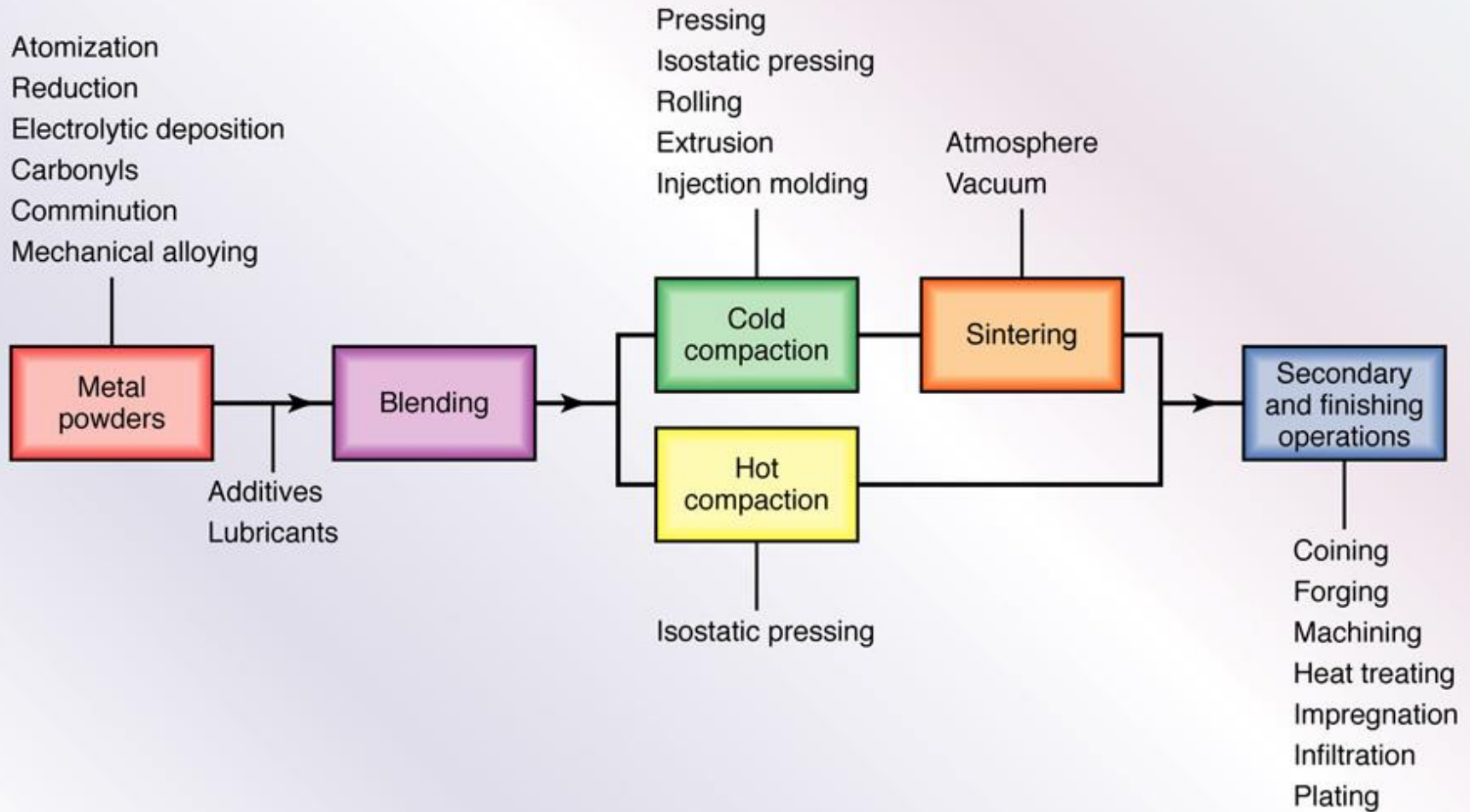
- %95 bağıl yoğunluklarda ürünlerin mekanik ve fiziksel özellikleri döküm ve benzeri yöntemlerle üretilen ürünlere benzerdir. Bazı yöntemlerle %99.9 bağıl yoğunluklara sahip ürünler elde etmek mümkündür.
- %90 ve üzeri bağıl yoğunluklara sahip ürünlere herhangi bir ek işleme gerek kalmadan kaplama yapılabilir.
- Gözenek oranını kontrol ederek titreşim ve gürültü özellikleri belirlenebilir.
- Rulman parçaları gibi aksamalarda kontrollü şekilde üretilmiş gözenekler sayesinde yağlayıcı tutuşu artar ve böylece aşınma azaltılır.
- Porozite kontrolü ile yağlayıcılık ve dayanım özellikleri arasında optimizasyon mümkündür.
- Kütle, hacim ve yoğunluk üzerindeki kontrol ile son yüzey özelliklerinin geliştirilmesi.
- Çatlama olmaksızın dövülebilen, bükülebilen parçalar üretilmesi.
- **Toz metalurjisi yöntemi sayesinde elmas içeren kesici porselenler, camlar, karbür kesici takımlar, refrakter metaller gibi diğer yöntemlerle üretilmesi mümkün olmayan malzemeler üretilmektedir.**
- **Reaktif ya da reaktif olmayan (yüksek ergime derecesine sahip & düşük ergime derecesine sahip) malzemeler üretilir.**

MMK Üretimi: Toz Metalurjisi

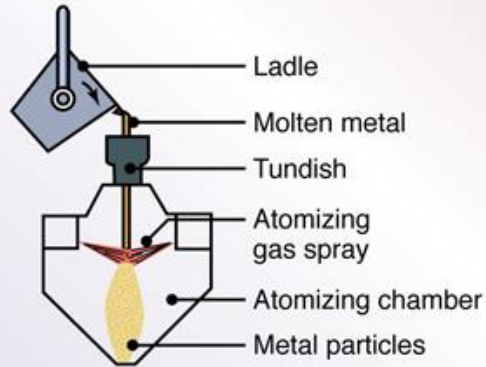
Dezavantajları:

- Genel olarak, boyutların çok büyük ya da şekillerin çok karmaşık olduğu durumlarda malzemeye bağlı olarak ya da presleme basınçlarının yüksekliğine bağlı olarak ortaya çıkan engeller.
- İlk yatırım maliyetlerinin, özellikle kalıpların maliyetinin, yüksekliği. Ekonomik olarak verimli olabilmesi için yıllık 10000'den fazla parça üretilmeli.
- Parçanın şekli ve ilgili kalıp tasarımı kalıba kolayca yerleşip çıkarılabilecek şekilde olmalı.
- Presleme sırasındaki uygulanan basınç malzeme alanını ve uzunluğunu etkilemektedir.
- Silindirik malzemeler üretilemez (kalıp tasarımlarından dolayı).
- Düşük ergime sıcaklığına sahip metallerin (kurşun, çinko, kalay vb.) sinterlenmesi hem zor hem de diğer yöntemlere göre yüksek maliyetlidir.

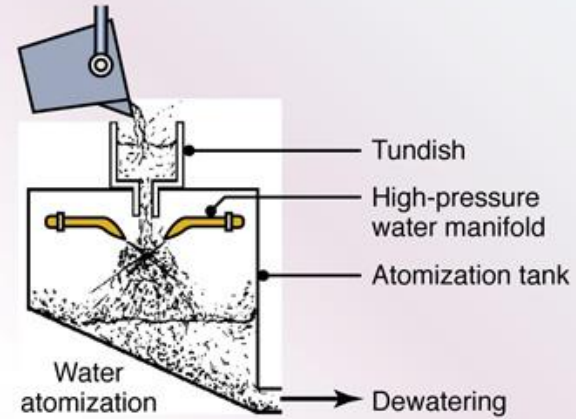
MMK Üretimi: Toz Metalurjisi



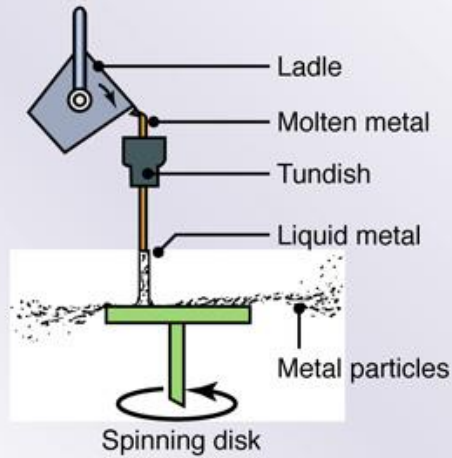
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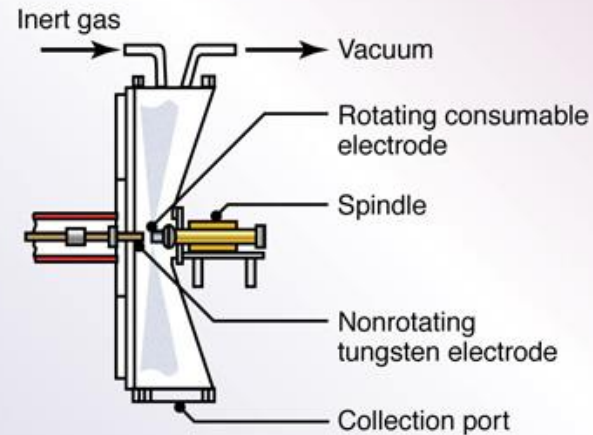
(a)



(b)

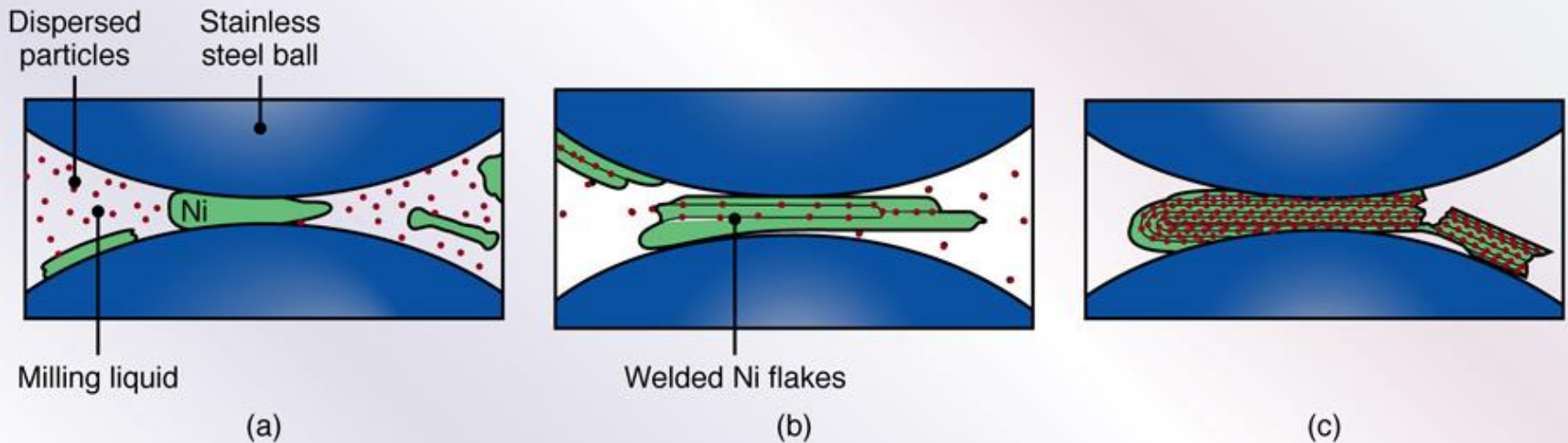
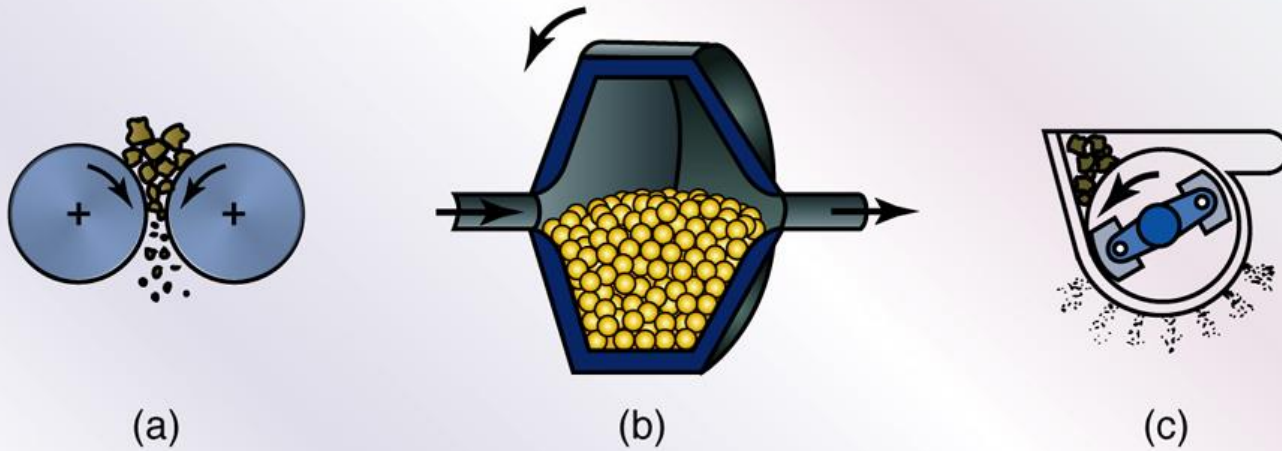


(c)



(d)

MMK Üretimi: Toz Metalurjisi



MMK Üretimi: Sinterleme

Sinter kelimesi Almanca kül anlamına gelmektedir.

Teknik anlamda sinterleme, metal ve/veya seramik tozlarına termal enerji uygulanması ile yoğunluk kontrollü malzemeler geliştirme prosesidir.

Diğer bir tanıma göre sinterleme, toz esaslı malzemelerin ana bileşenin ergime sıcaklığının altında sıcaklıklara ısıtılması ile tozların biraraya gelerek dayanımı yüksek ürünler elde edilmesi işlemidir.

Katı faz sinterlemesi, sıvı faz sinterlemesi ve reaktif sinterleme olarak üç ana başlık altında toplamak mümkündür.

Sinterleme sırasında basınç uygulanıp uygulanmadığına göre de basınçsız sinterleme ve basınçlı sinterleme olarak iki sınıfa ayırmak mümkündür.

MMK Üretimi: Sinterleme

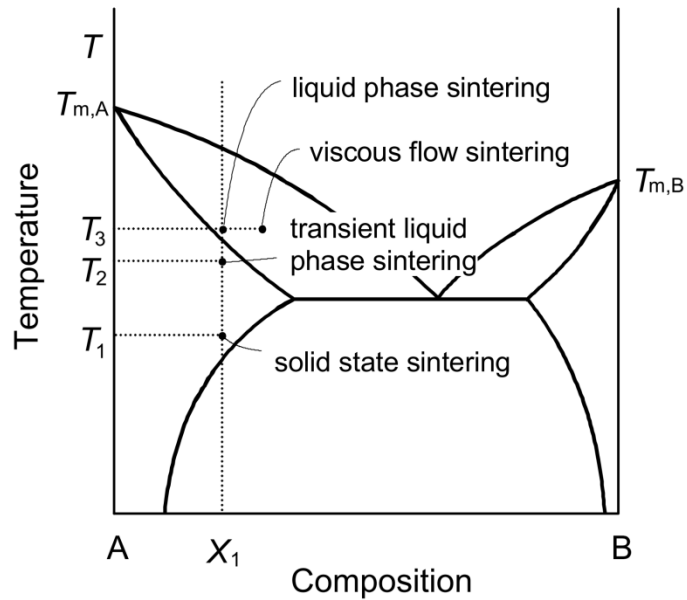


Figure I.3. Illustration of various types of sintering.

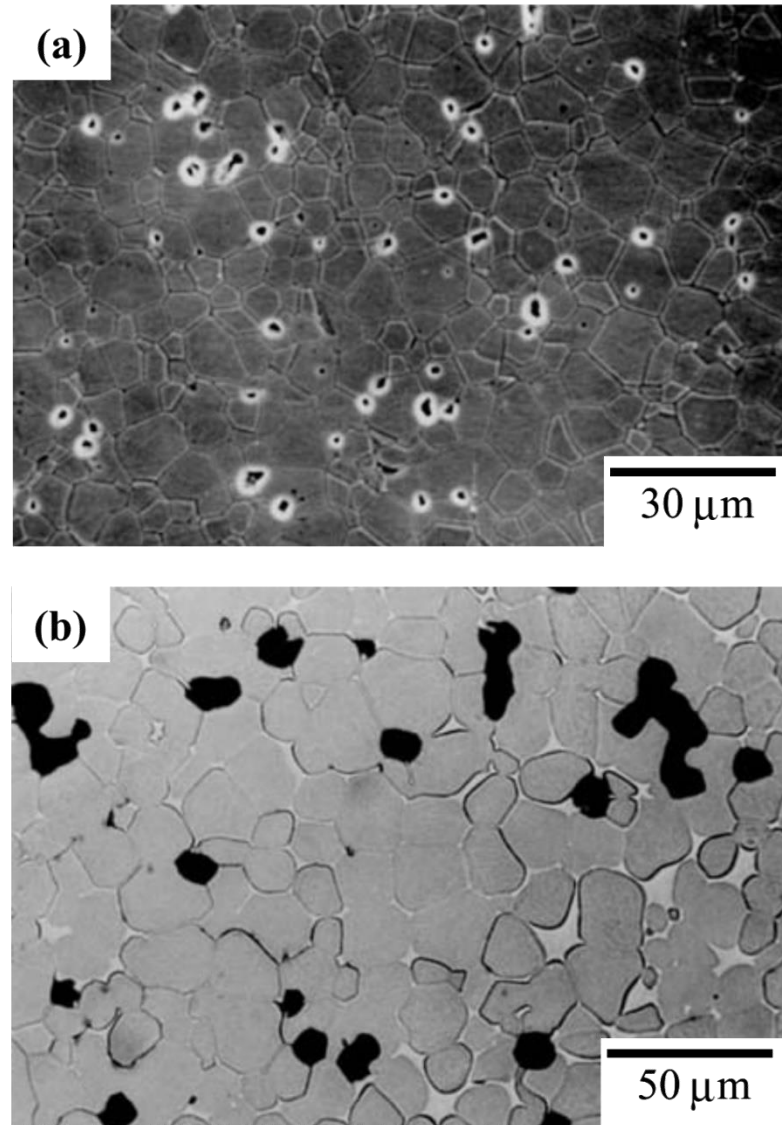


Figure I.4. Typical microstructures observed during (a) solid state sintering (Al_2O_3) and (b) liquid phase sintering (98W-INi-IFe(wt%)).

MMK Üretimi: Sinterleme

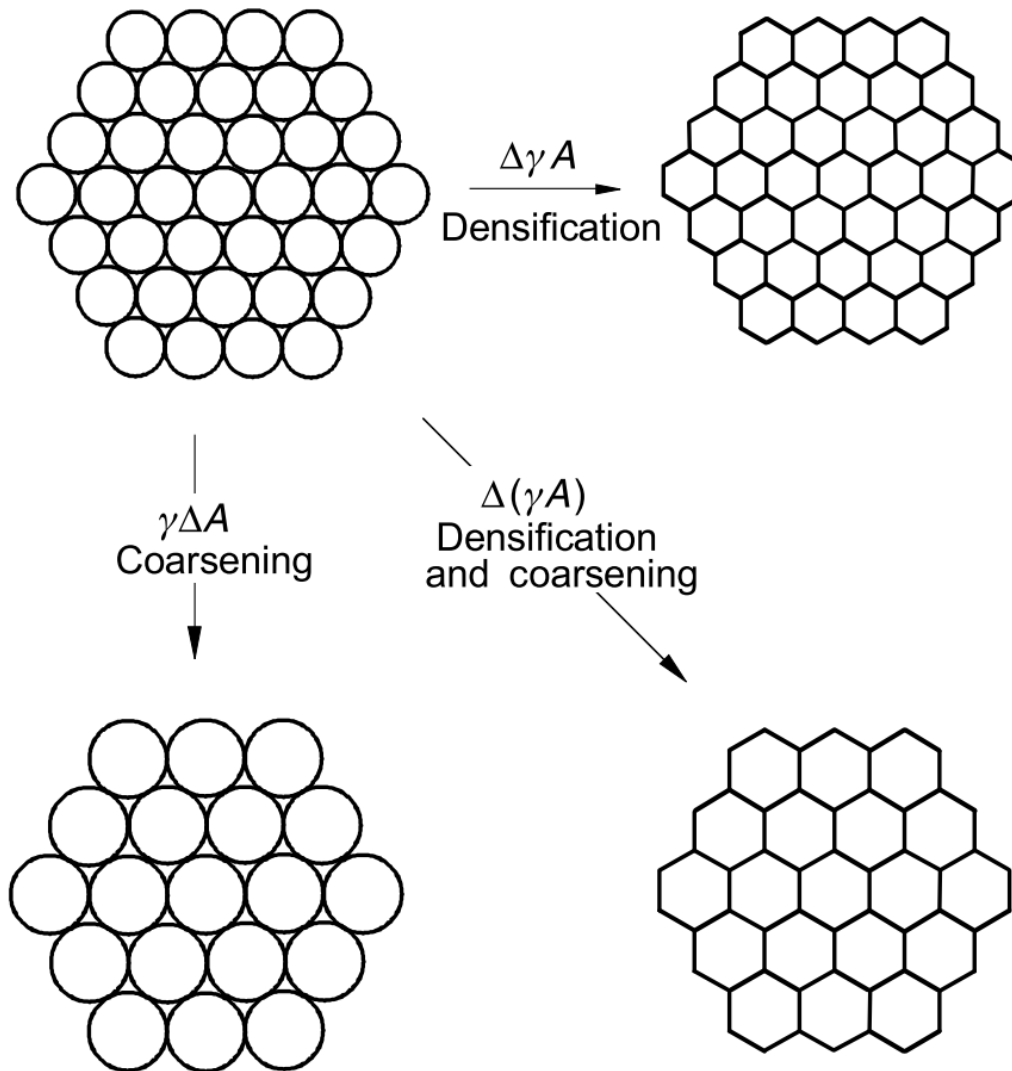


Figure I.5. Basic phenomena occurring during sintering under the driving force for sintering, $\Delta(\gamma A)$.

MMK Üretimi: Sinterleme

Table I.I. Variables affecting sinterability and microstructure

Variables related to raw materials (material variables)	Powder: shape, size, size distribution, agglomeration, mixedness, etc. Chemistry: composition, impurity, non-stoichiometry, homogeneity, etc.
Variables related to sintering condition (process variables)	Temperature, time, pressure, atmosphere, heating and cooling rate, etc.

- 1. Toz Hazırlama Aşamasında:** Parçacık boyutu, şekli, boyut dağılımı.
- 2. Çok Bileşenli Sistemlerde:** İkincil fazların dağılımı
- 3. Toz Presleme Aşamasında:** Ham yoğunluk, gözenek boyutu dağılımı
- 4. Sinterleme Aşamasında:** Sinterleme sıcaklığı, ısıtma hızları, sinterleme süresi, uygulanan basınç, sinterleme atmosferi.

MMK Üretimi: Sinterleme

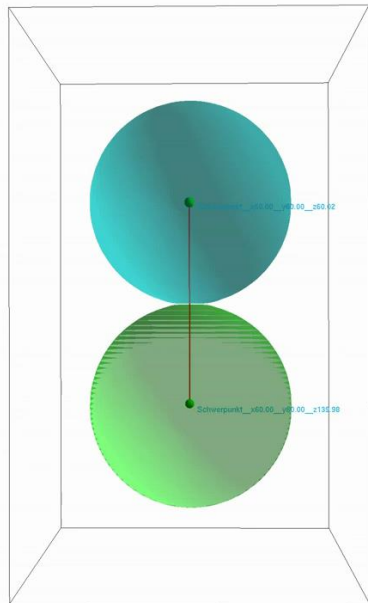
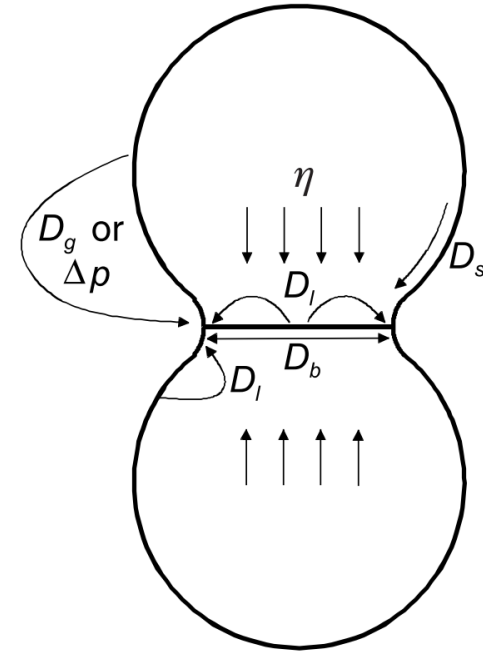
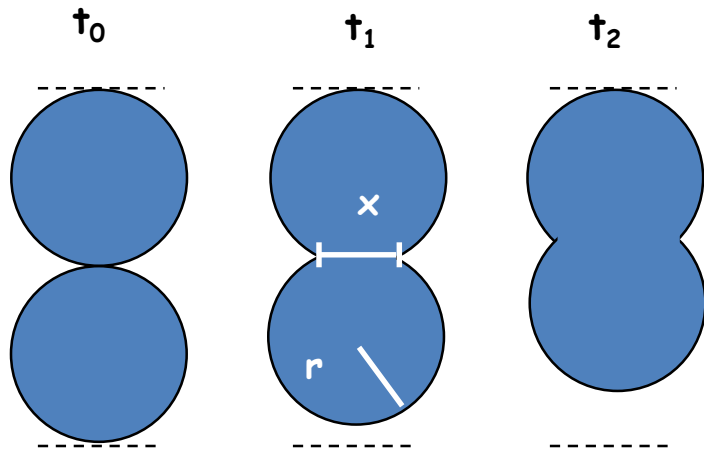
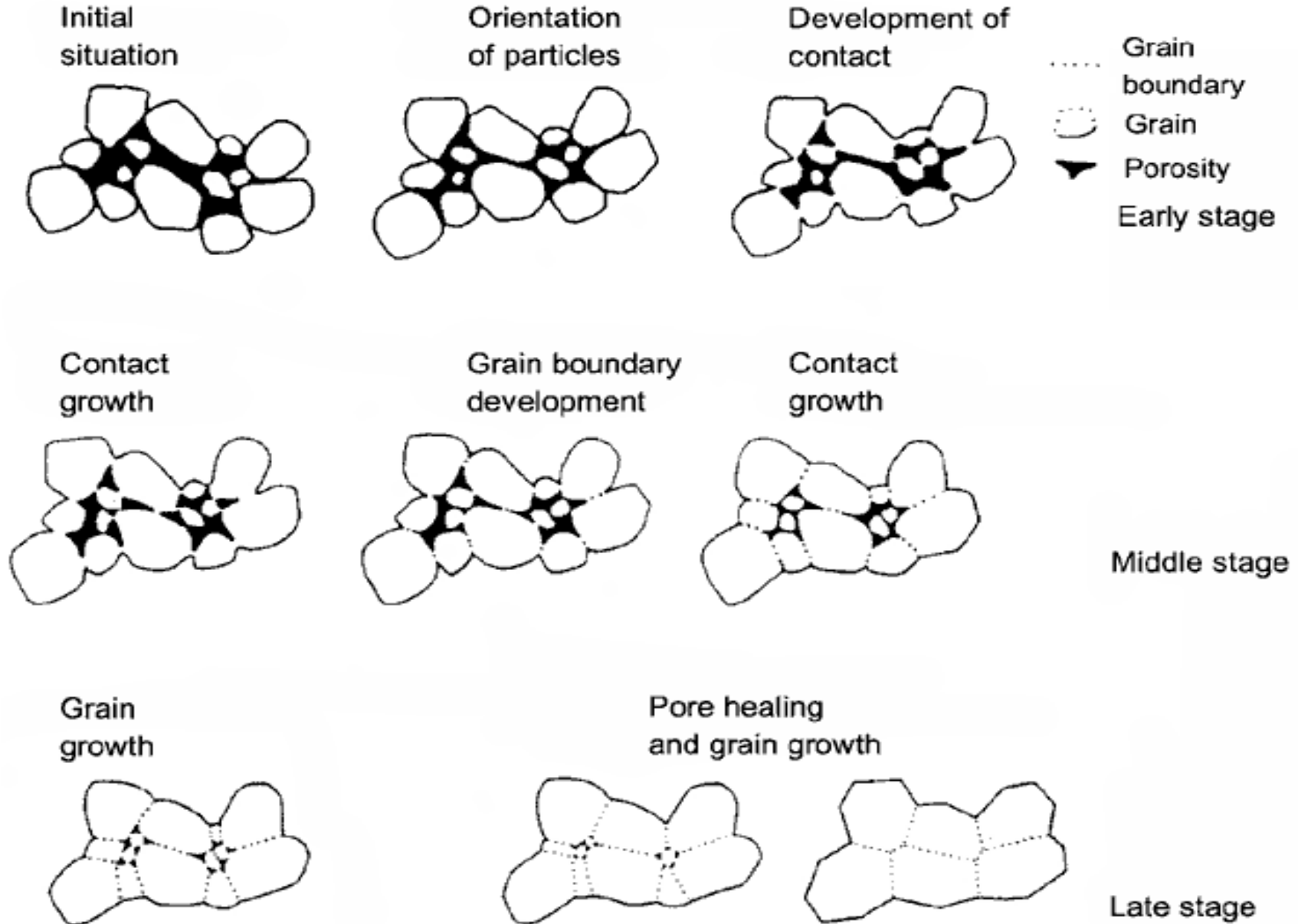


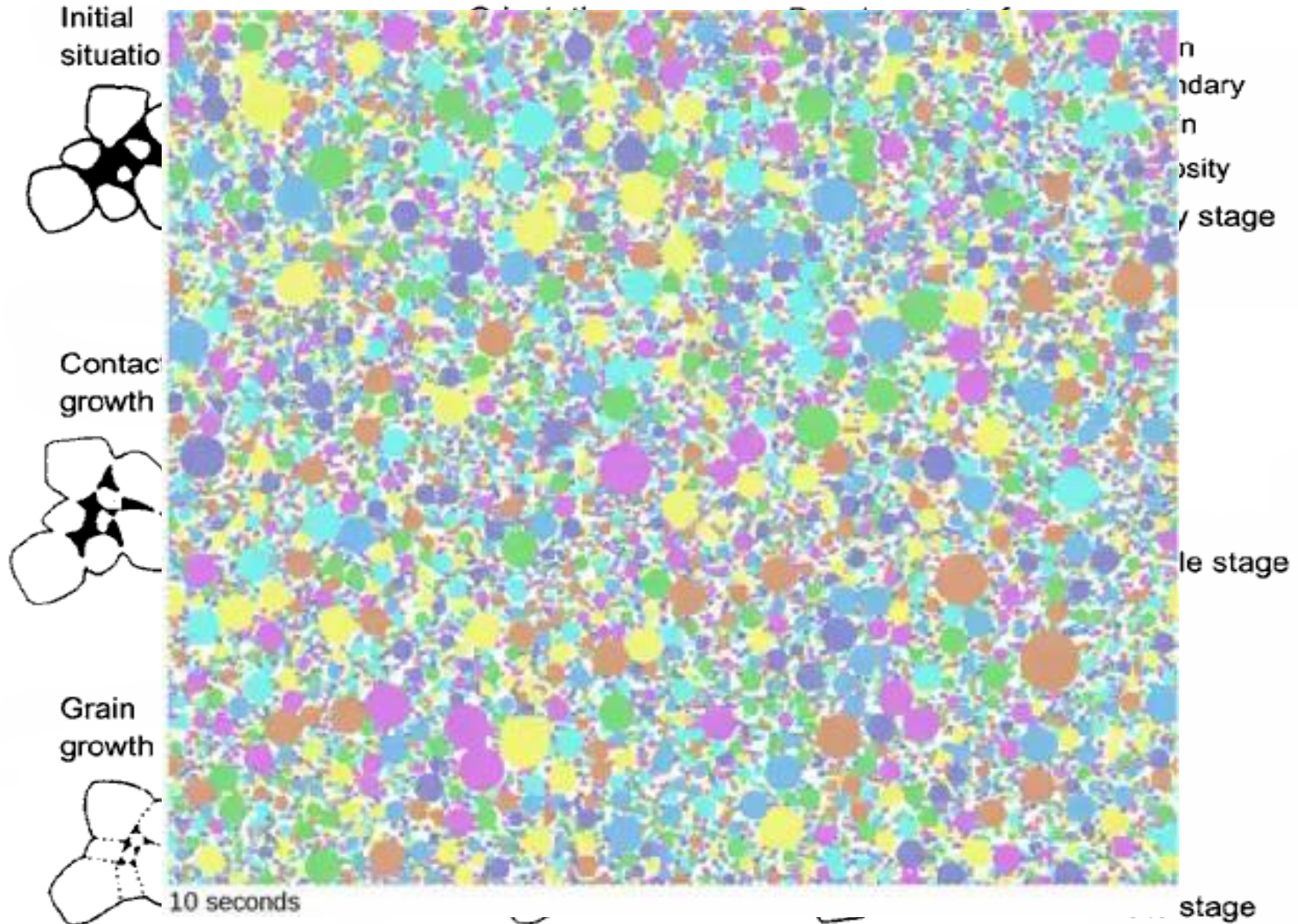
Table 4.I. Material transport mechanisms during sintering

Material transport mechanism	Material source	Material sink	Related parameter
1. Lattice diffusion	Grain boundary	Neck	Lattice diffusivity, D_l
2. Grain boundary diffusion	Grain boundary	Neck	Grain boundary diffusivity, D_b
3. Viscous flow	Bulk grain	Neck	Viscosity, η
4. Surface diffusion	Grain surface	Neck	Surface diffusivity, D_s
5. Lattice diffusion	Grain surface	Neck	Lattice diffusivity, D_l
6. Gas phase transport			
6.1. Evaporation/condensation	Grain surface	Neck	Vapour pressure difference, Δp
6.2. Gas diffusion	Grain surface	Neck	Gas diffusivity, D_g

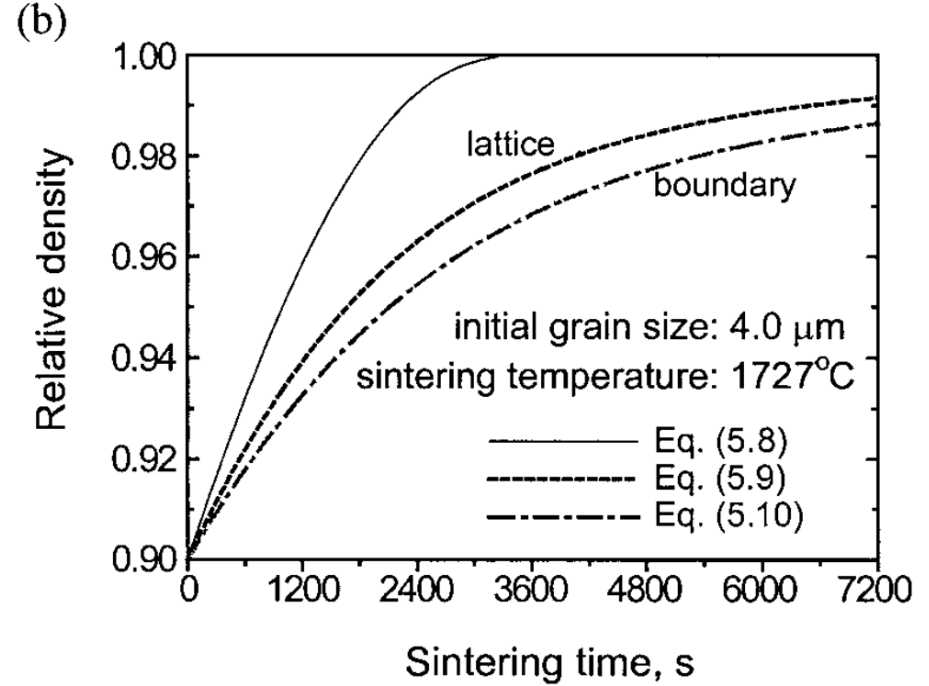
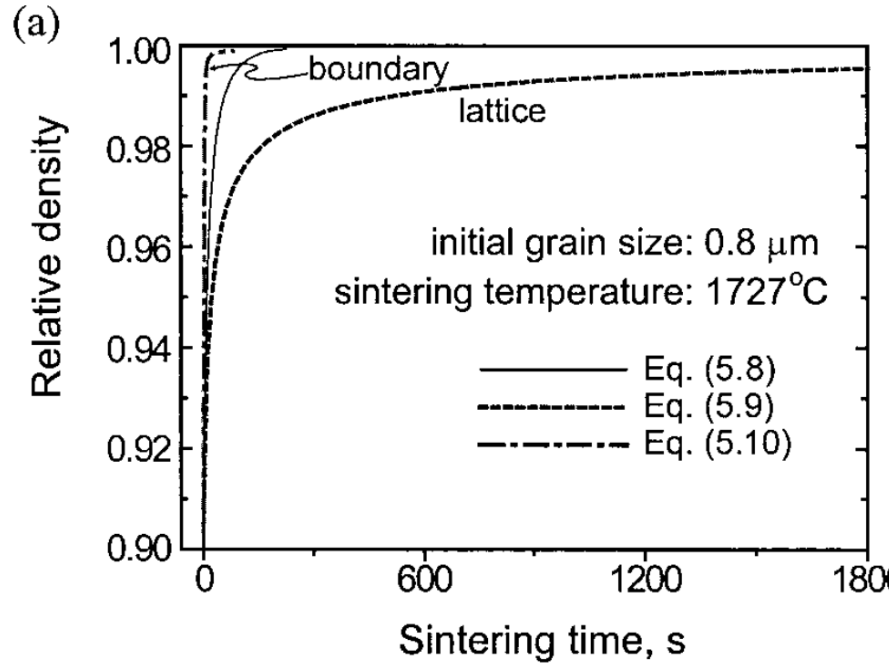
MMK Üretimi: Sinterleme



MMK Üretimi: Sinterleme

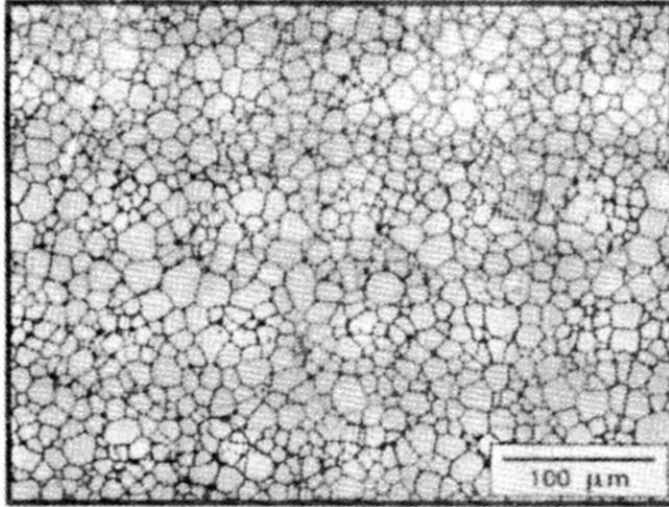


MMK Üretimi: Sinterleme

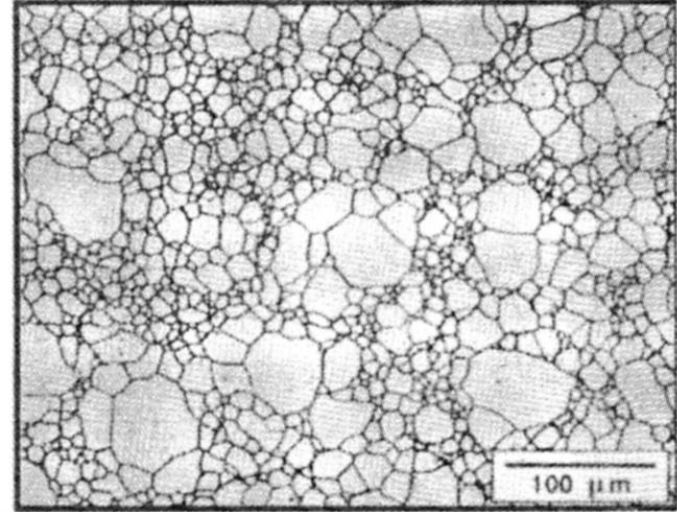


1727 derecede sinterlenen Al_2O_3 için hesaplanmış sinterleme süresi
yoğunluk grafikleri

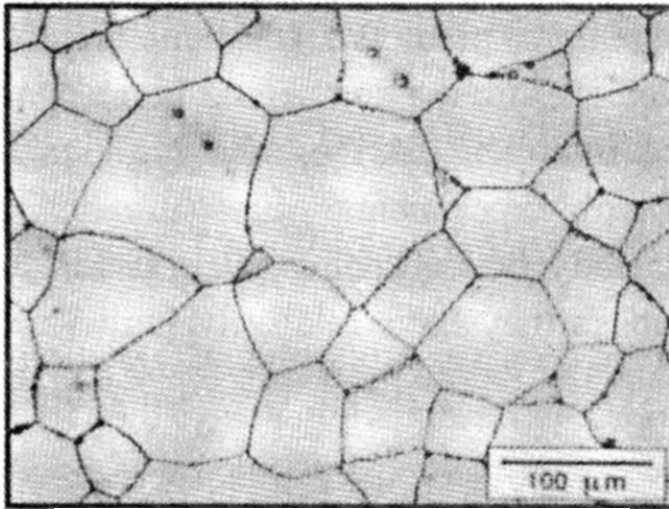
MMK Üretimi: Sinterleme



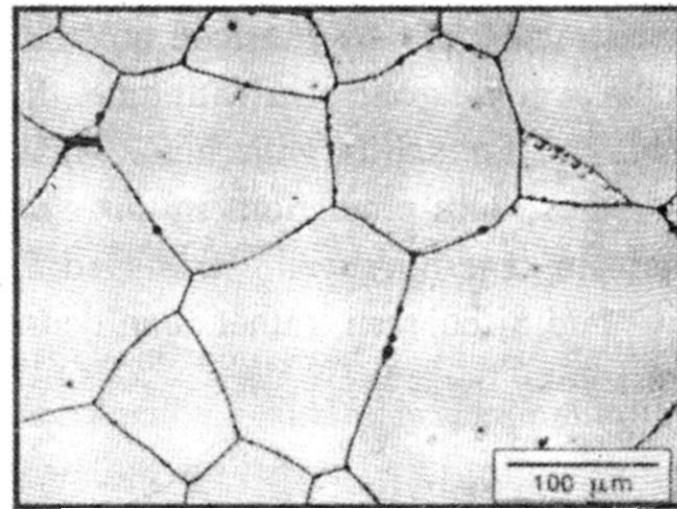
5 dakika



20 dakika



60 dakika



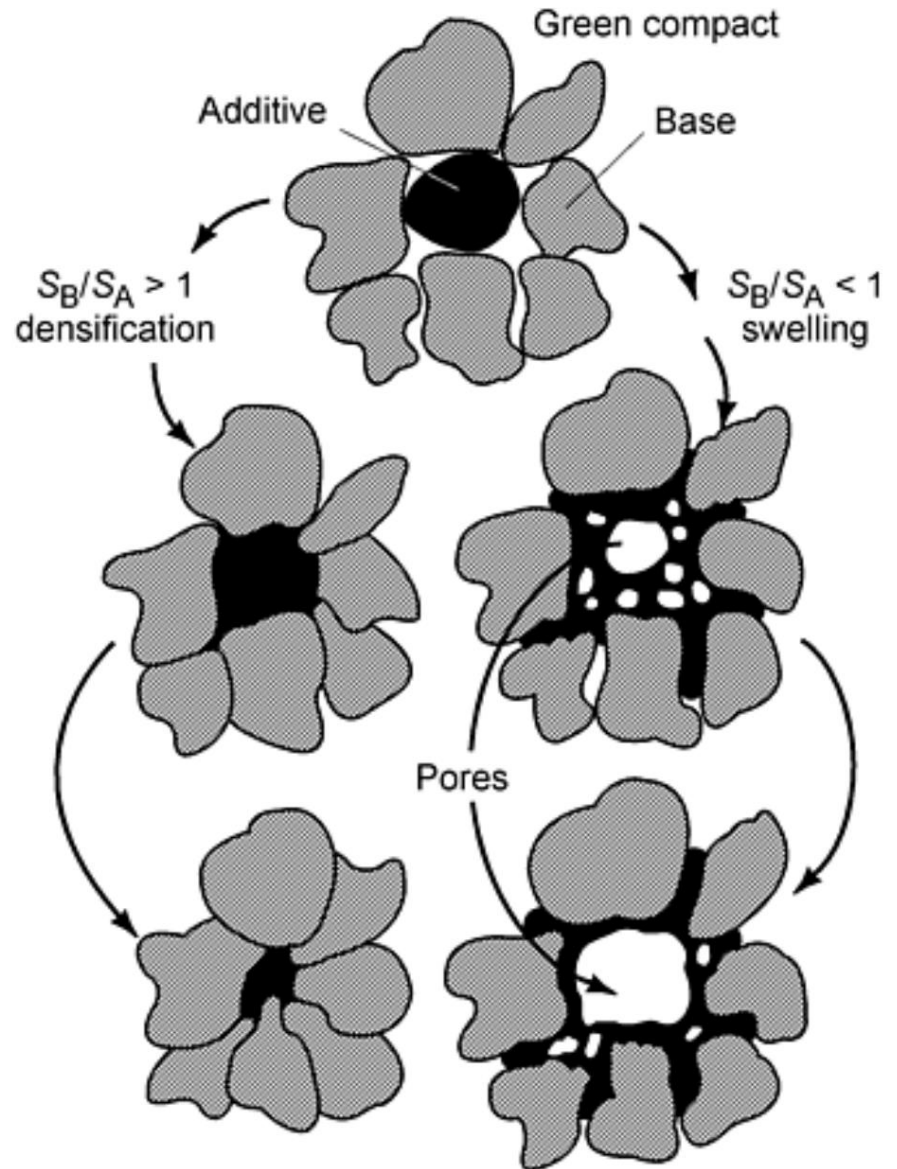
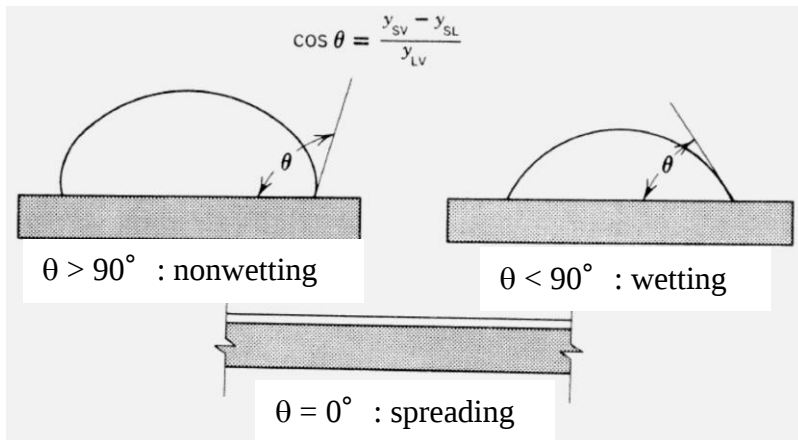
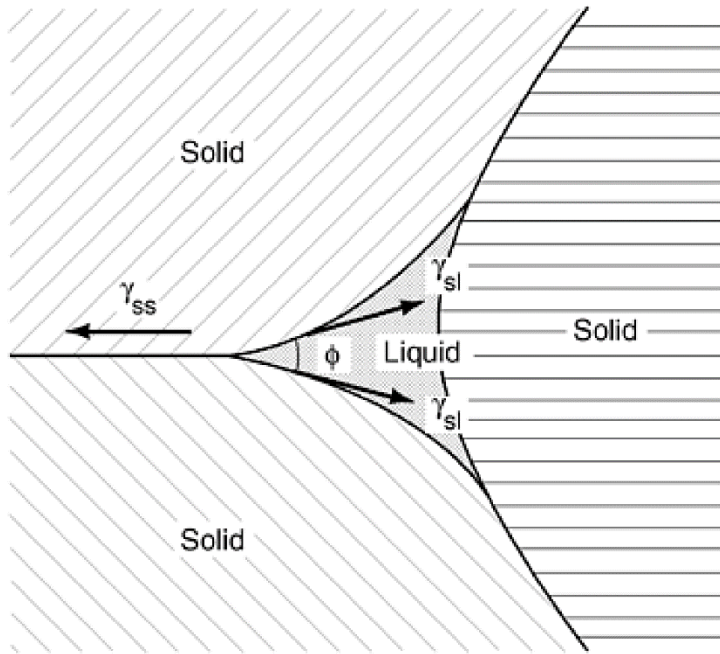
120 dakika

MMK Üretimi: Sinterleme

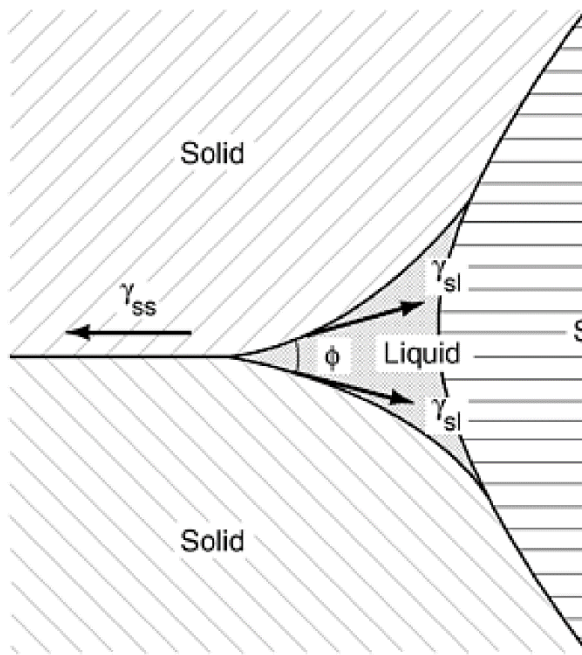
Sintered material	Sintering temperatures, °C
Aluminum alloys	590-620
Bronze	740-780
Brass, 890-910	
Iron, carbon steels, low-alloyed steels (Cu, Ni)	1120-1150
Low-alloyed steels (Cu, Ni, Mo; Distaloy)	1120-1200
High-alloyed ferritic and austenitic steels (Cr, Cr-Ni)	1200-1280
Hard magnets (Alnico)	1200-1350
Hard metals (cemented carbides)^(a)	1350-1450
Molybdenum and molybdenum-alloys	1600-1700
Tungsten^(b)	200-2300
Heavy metal (W alloy)	~1400
Ferrites (soft and hard)	1100-1300
Silicon nitride (with different additives)^(c)	1750-2000
Silicon carbide (with different additives)^{(d)(e)}	1750-2100
Alumina^(e)	1400-1800
Zirconia (with different additives)^(e)	1400-1750

- (a) TiC-based hard metals (cermets) up to 1600 °C.
- (b) ~3000 °C, when direct sintering is used.
- (c) Highest temperature under pressured N₂ atmosphere or in powder bed.
- (d) Low temperatures for liquid phase sintering.
- (e) Low temperatures for highly active powders.

MMK Üretimi: Sinterleme

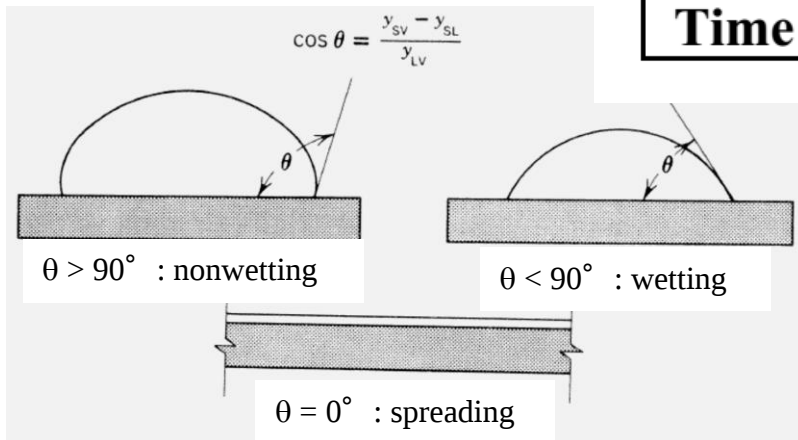


MMK Üretimi: Sinterleme



Factor	Swelling	Shrinkage
Solid solubility in liquid	Low	High
Liquid solubility in solid	High	Low
Diffusivities	Unequal	Equal
Additive particle size	Large	Small
Base particle size	Large	Small
Green density	High	Low
Contact angle	High	Low
Dihedral angle	High	Low
Temperature	Low	High
Time	Short	Long

 Green compact



MMK Üretimi: Sinterleme

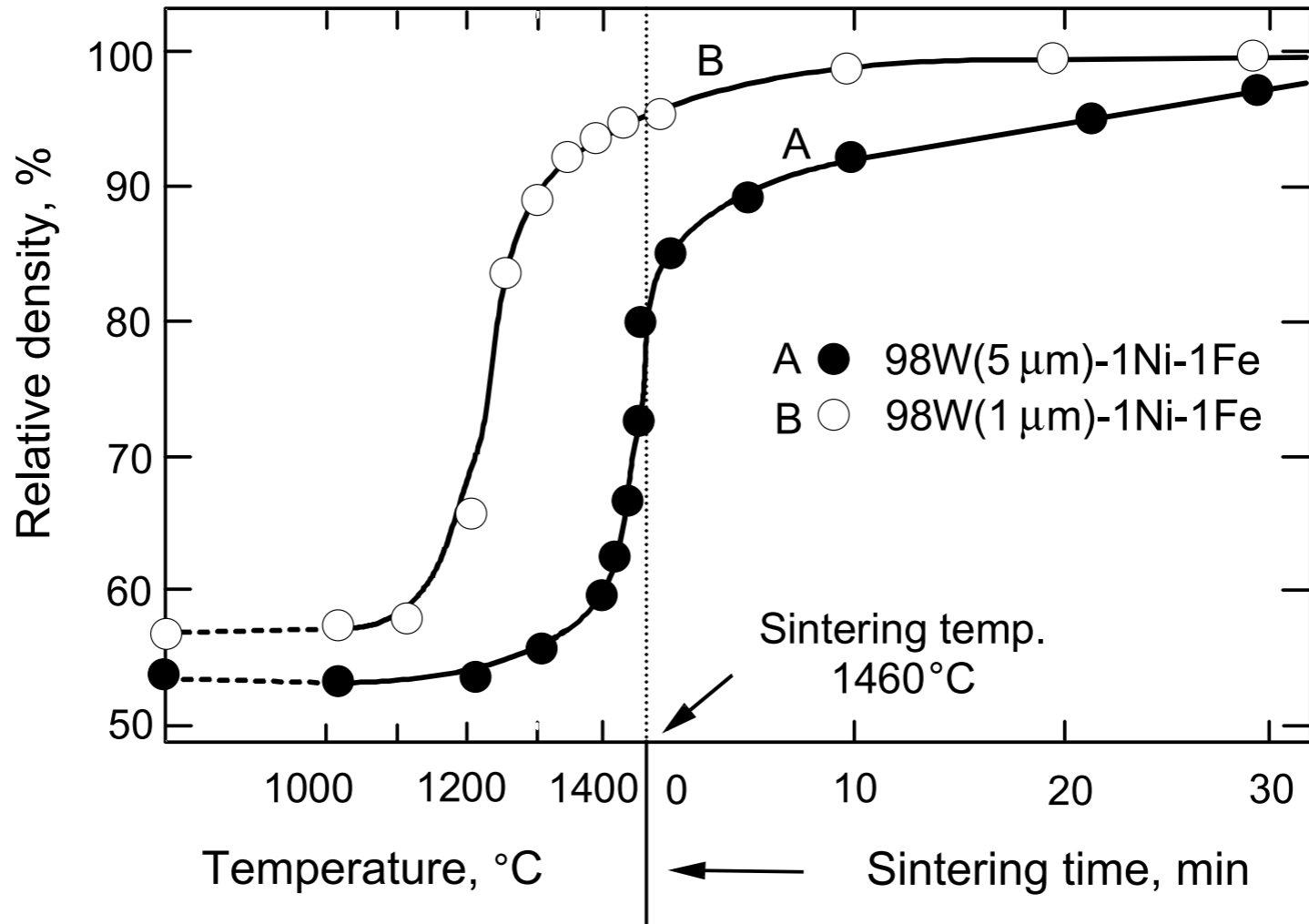


Figure I4.I. Densification curves of 98W-1Ni-1Fe(wt%) alloys during heating to and isothermal liquid phase sintering at 1460°C.¹

MMK Üretimi: Sinterleme

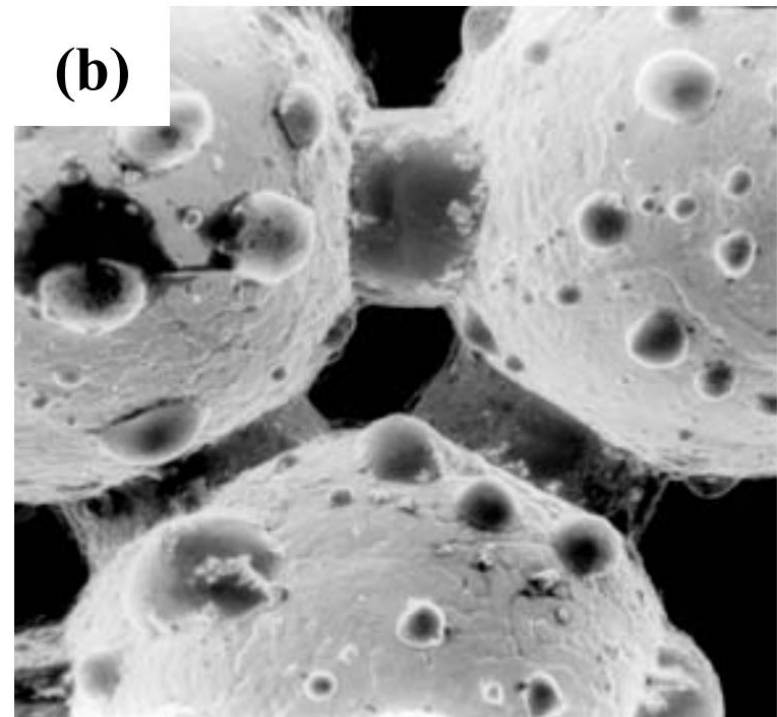
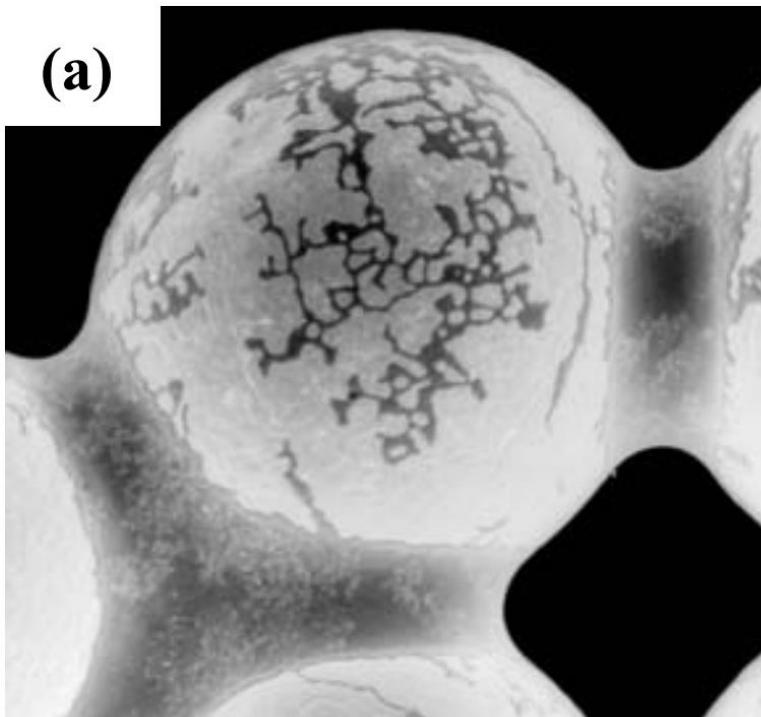
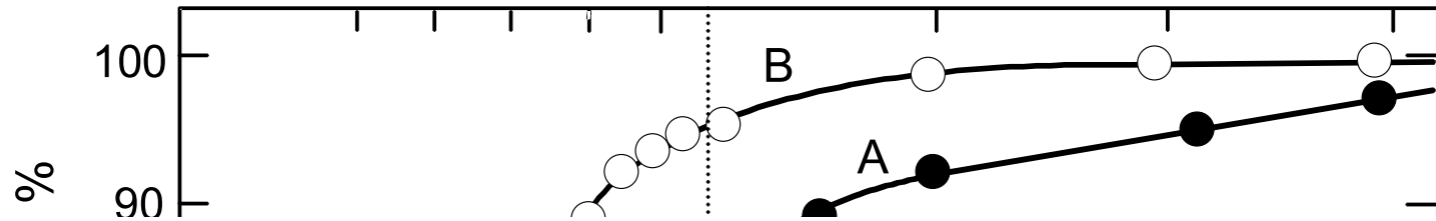


Figure 14.5. Distribution of liquid Cu between W spheres ($\sim 200 \mu\text{m}$ diameter) for a wetting angle θ of (a) 8° and (b) 85° .²

Örnekler



Fig. 11. Electron micrograph of the fine powder from the Ti-25Al-10Nb-3V-1Mo (at.%) + 2 wt.% Er alloy powder mechanically alloyed and HIPed. Note the uniform distribution of the Er_2O_3 dispersoids in the Ti-matrix.

Örnekler

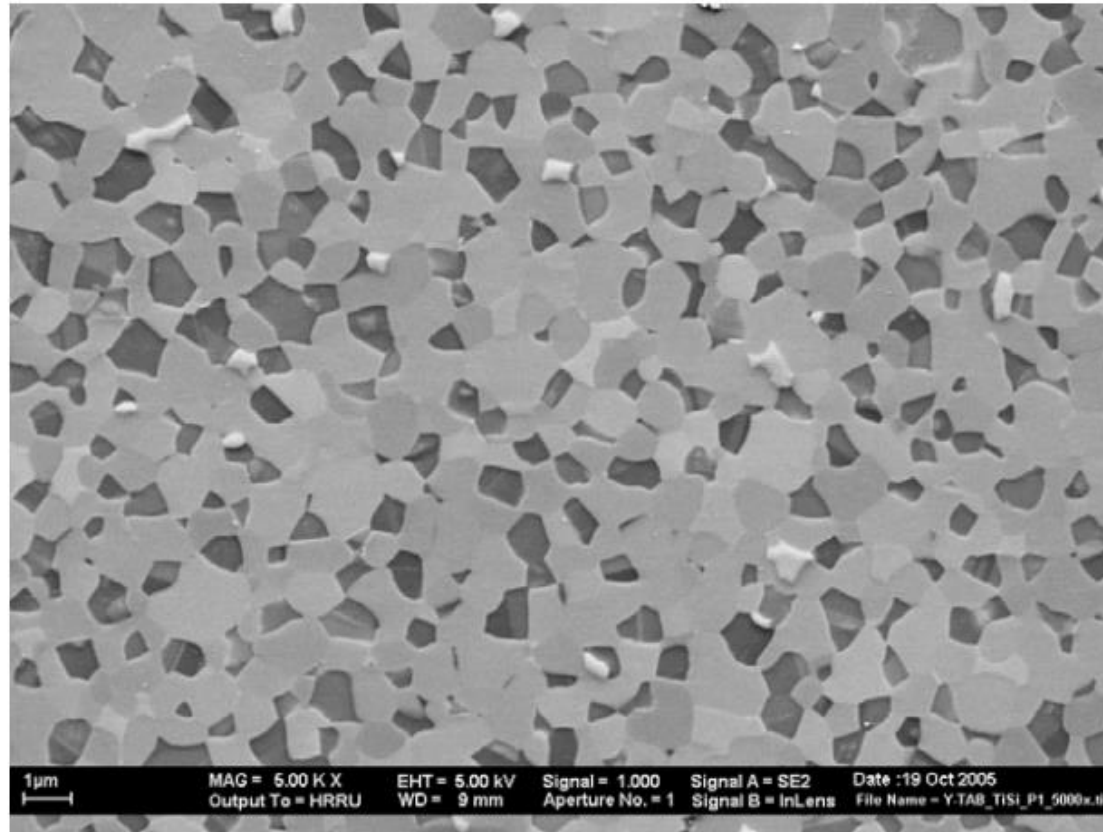


Fig. 14. Scanning electron micrograph of the γ -TiAl + 60 vol.% ζ -Ti₅Si₃ composite specimen showing that the two phases are very uniformly distributed in the microstructure. Such a microstructure is conducive to observing superplastic deformation under appropriate conditions of testing.

Örnekler

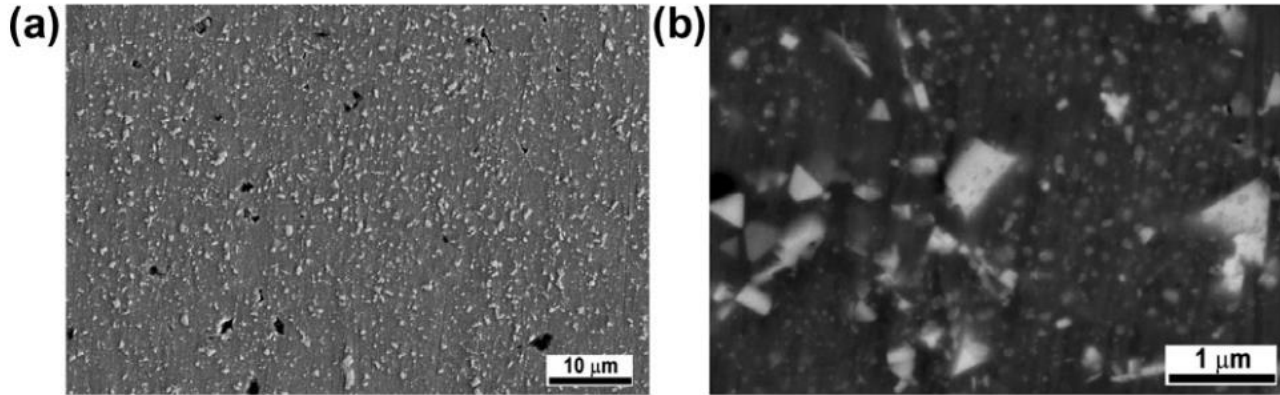
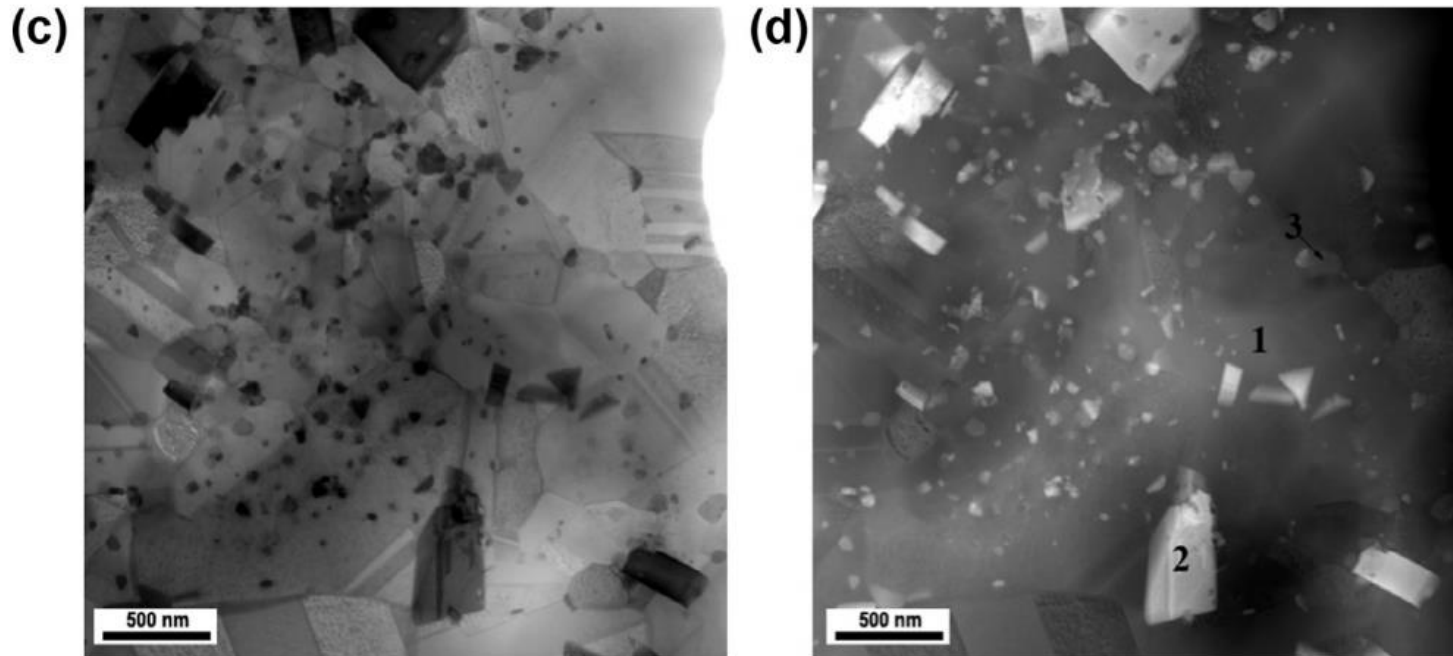


Fig. 6. SEM micrographs taken from the SPS-1000-hBN sample: (a) Low magnification secondary electron image and (b) high magnification back scattered electron image.



Ni(W) – WC kompozitleri

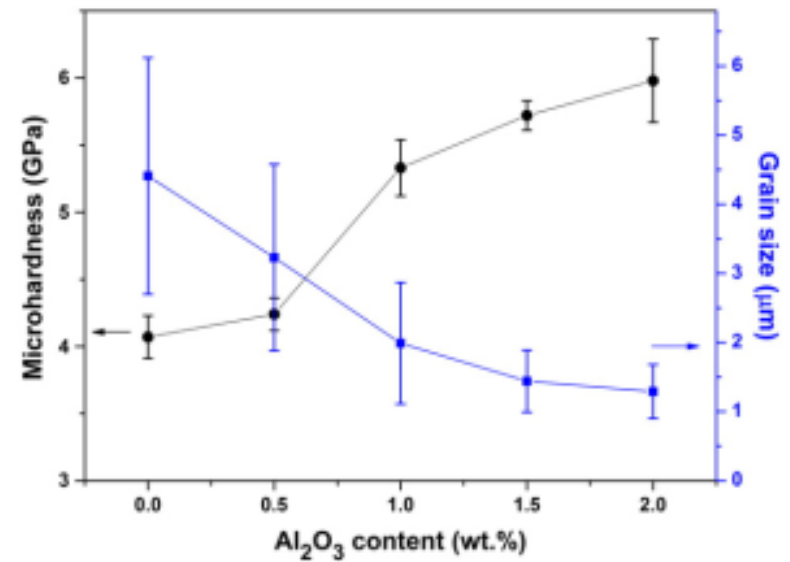
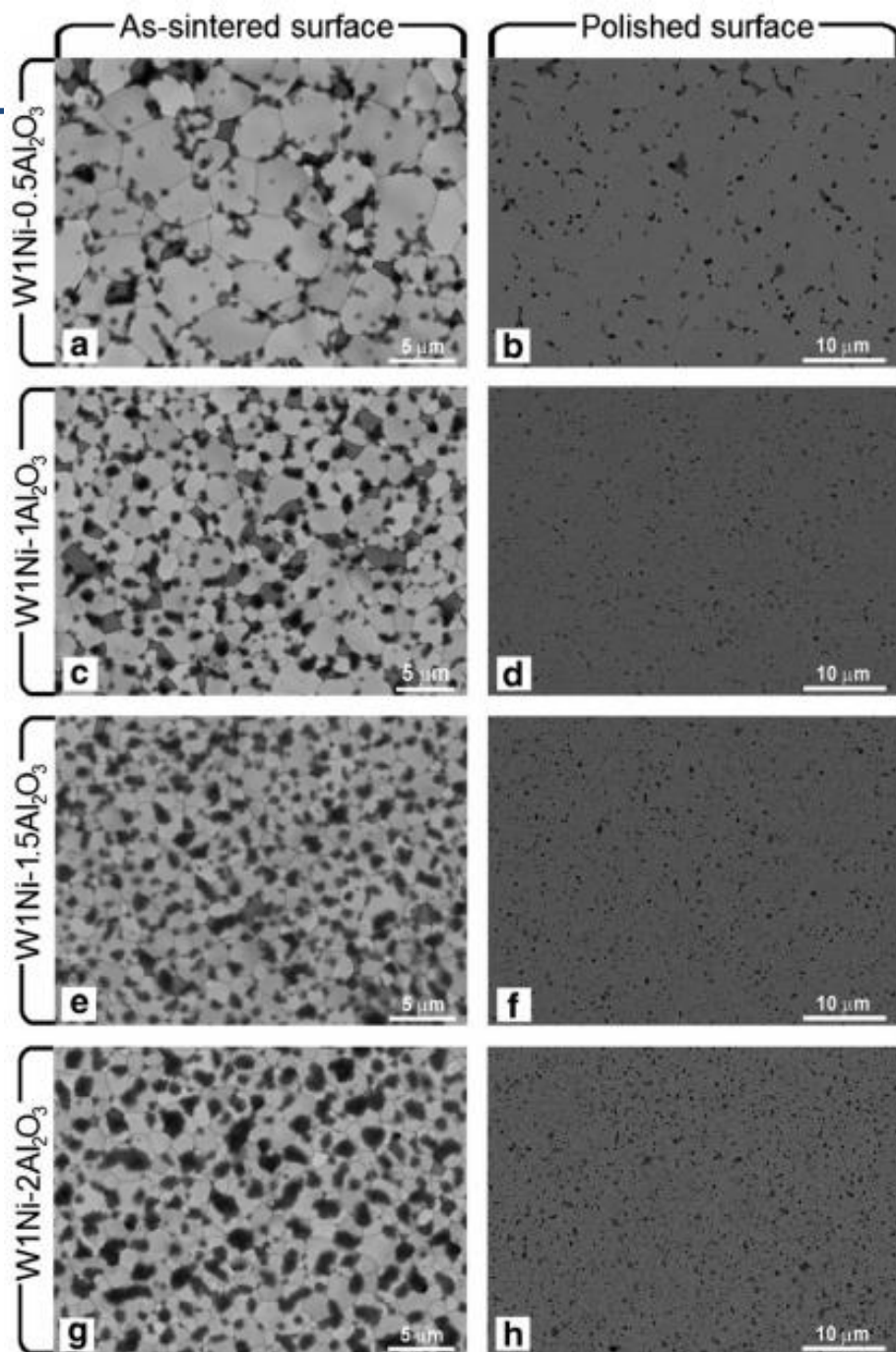
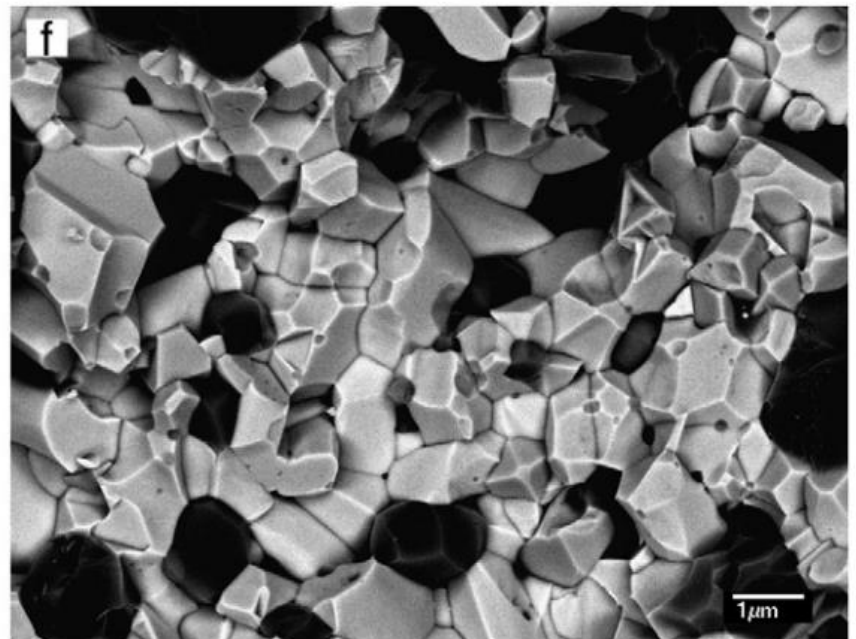
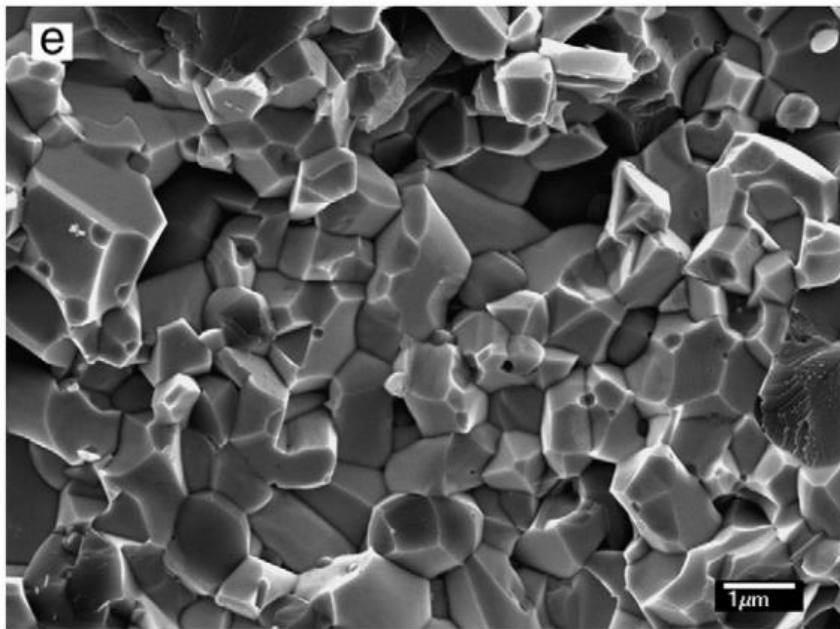
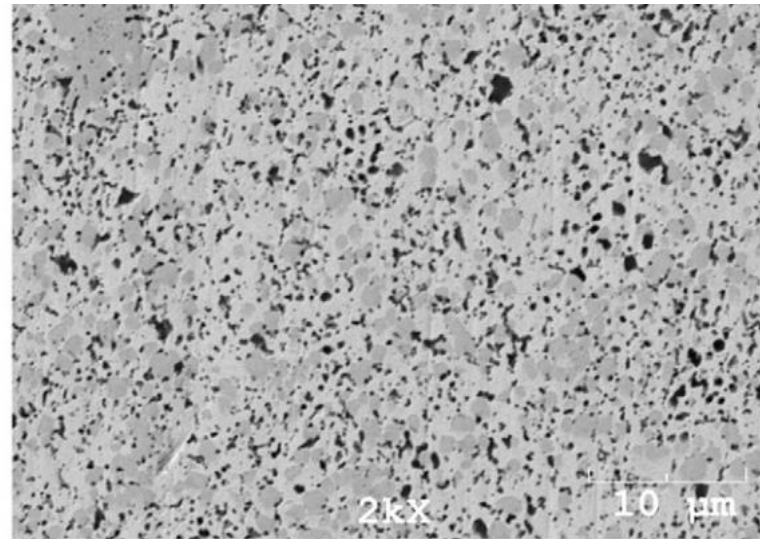
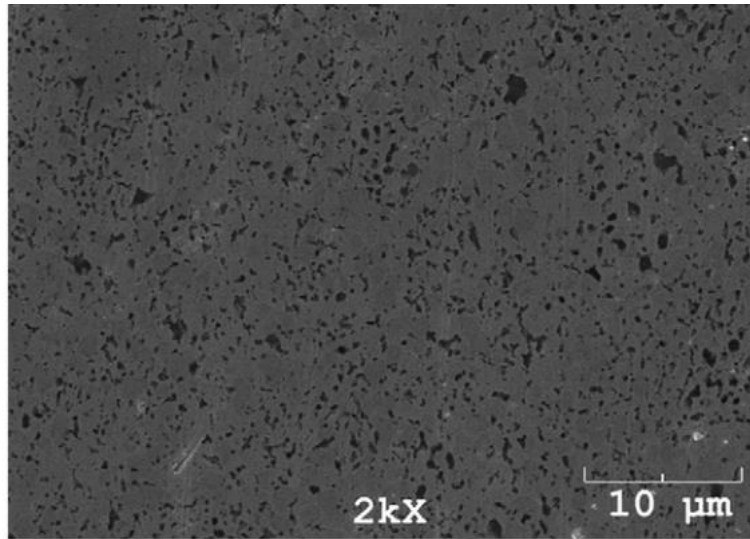


Fig. 6. Evolution of microhardness values and average W grain size with the addition of Al₂O₃ particles.

Örnekler

(e) $\text{W}_{10}\text{Ni}_{1.5}\text{Y}_2\text{O}_3 + 5\text{TiB}_2$ samples and (f) is corresponding BEI micrograph of (e).

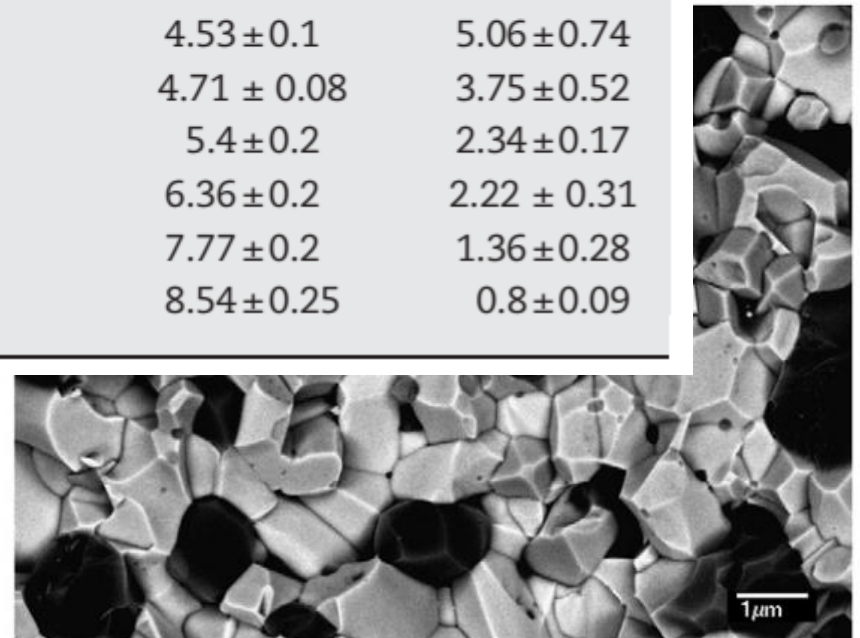
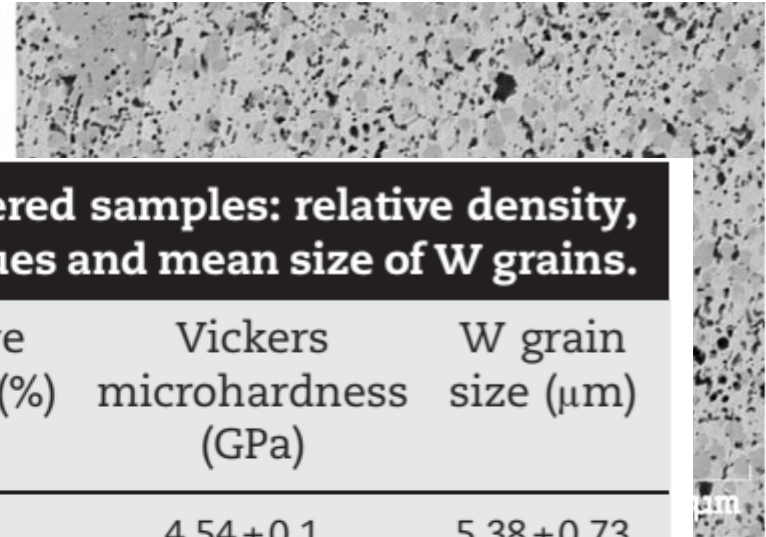
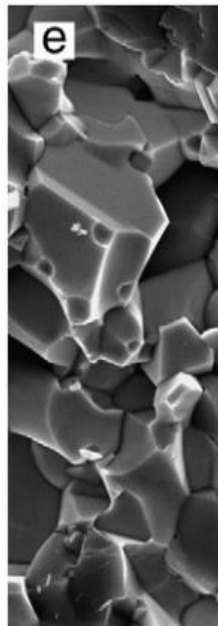


Örnekler

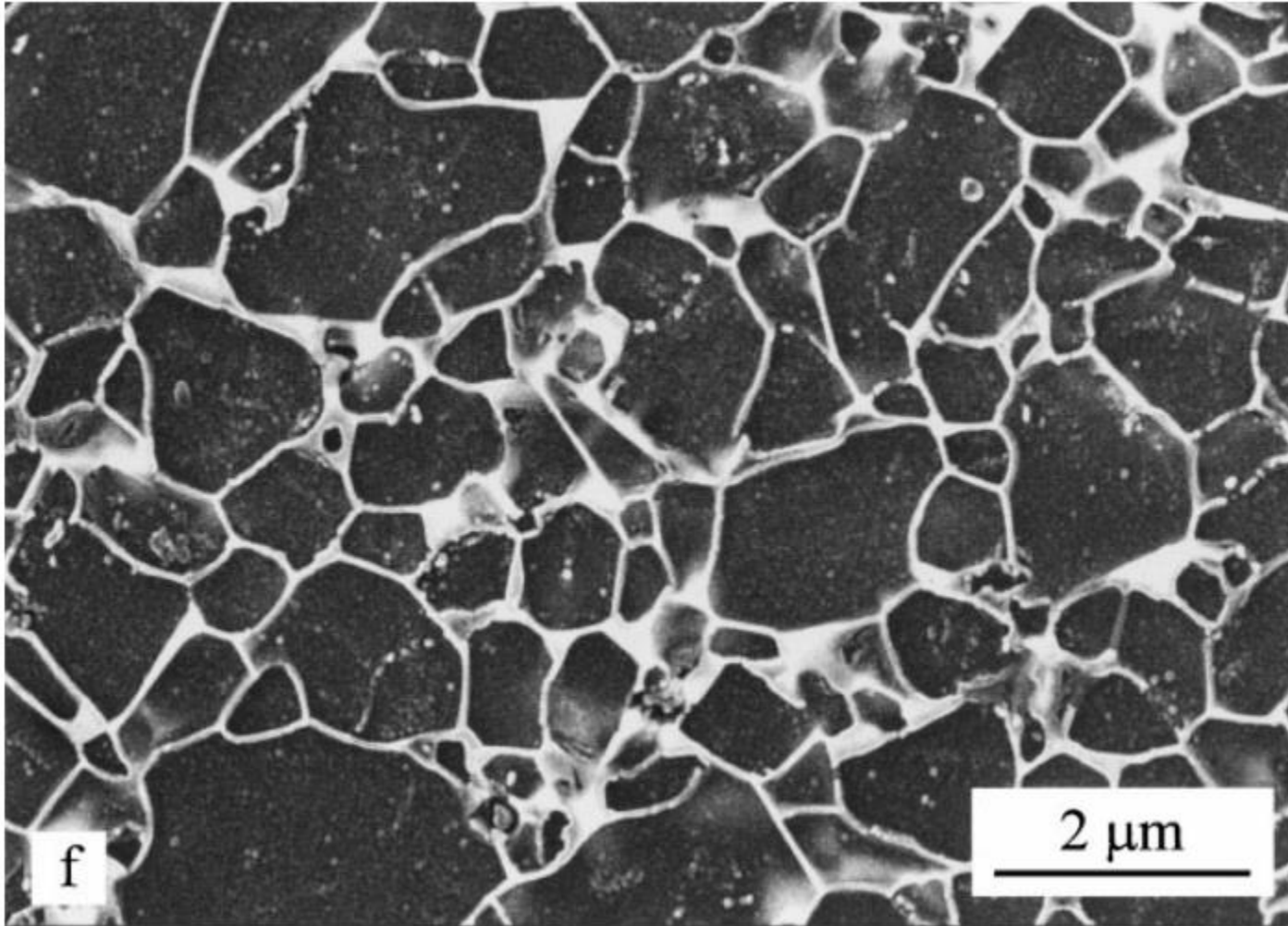
(e) $\text{W1Ni0.5Y}_2\text{O}_3 + 5\text{TiB}_2$ samples and (f) is corresponding BEI micrograph of (e).

Table 1 – Properties of sintered samples: relative density, Vickers microhardness values and mean size of W grains.

Sample	Relative density (%)	Vickers microhardness (GPa)	W grain size (μm)
W1Ni	97.03	4.54 ± 0.1	5.38 ± 0.73
W1Ni0.5Y ₂ O ₃	95.43	4.53 ± 0.1	5.06 ± 0.74
W1Ni0.5Y ₂ O ₃ + 1TiB ₂	96.27	4.71 ± 0.08	3.75 ± 0.52
W1Ni0.5Y ₂ O ₃ + 2TiB ₂	95.71	5.4 ± 0.2	2.34 ± 0.17
W1Ni0.5Y ₂ O ₃ + 3TiB ₂	97.31	6.36 ± 0.2	2.22 ± 0.31
W1Ni0.5Y ₂ O ₃ + 4TiB ₂	95.43	7.77 ± 0.2	1.36 ± 0.28
W1Ni0.5Y ₂ O ₃ + 5TiB ₂	95.67	8.54 ± 0.25	0.8 ± 0.09

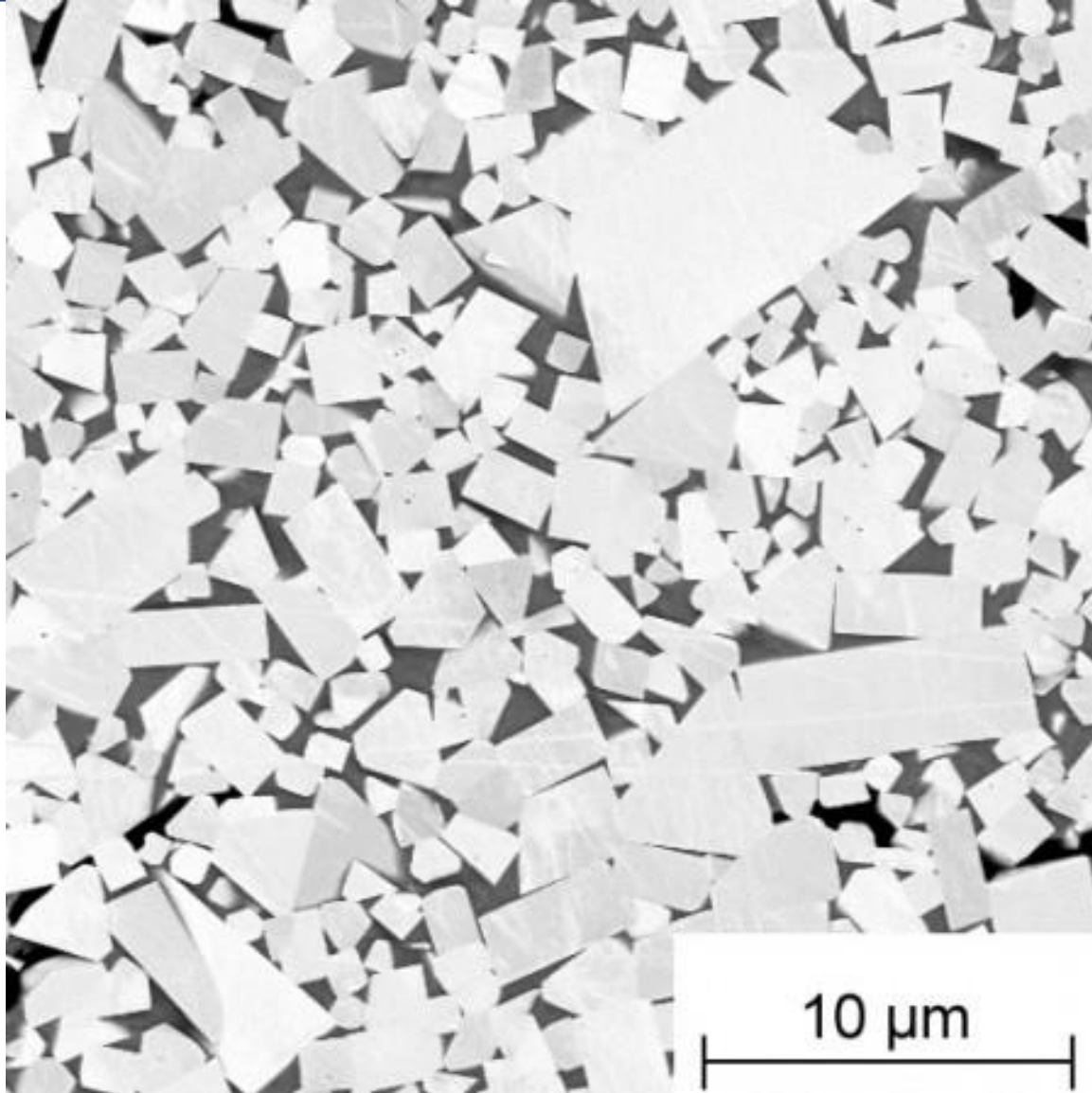


Örnekler



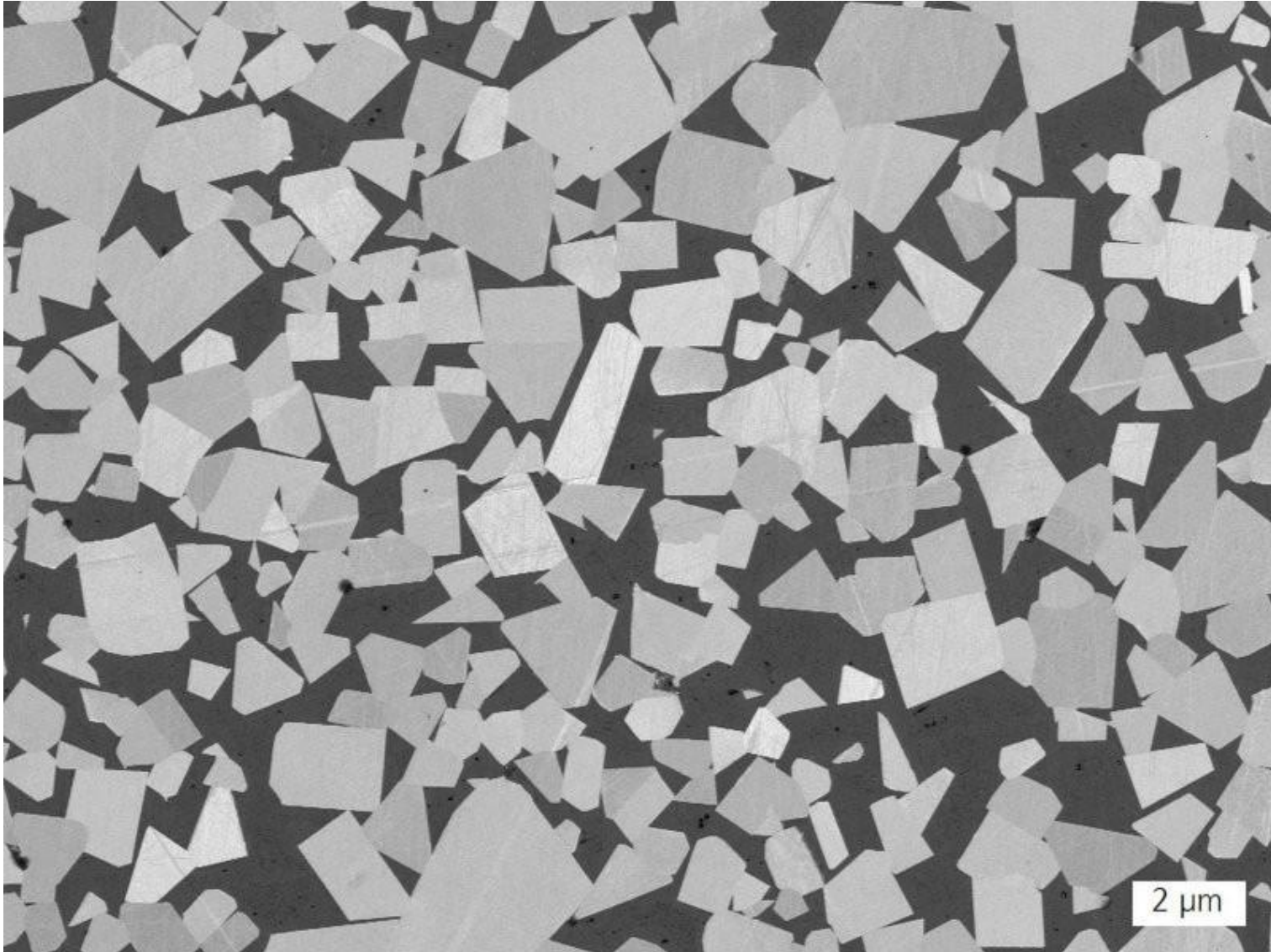
Sıvı faz sinterlemesi ile üretilmiş $\text{Y}_2\text{O}_3\text{-Al}_2\text{O}_3$ katkılı SiC

Örnekler



Sıvı faz sinterlemesi ile üretilmiş WC-Co sert metali

Örnekler



Sıvı faz sinterlemesi ile üretilmiş WC-Co sert metali

Kaynaklar:

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